LARA EXPLORATION LTD.

Summary of Exploration, Metallurgical and

Scoping Studies Performed on the Lara Porphyry

Copper Property and Proposed 2005

Exploration Program

Rio Viscus

Palpa, Peru

by

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February 9, 2004
(Revised March 31, 2005)

Gibsons, British Columbia

PGS Pacific Geological Services

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Summary

The Lara property is located about 40 km east of the Pan American Highway, 400 km southeast from Lima, Peru. The claims are 100% owned by Minas Dixon S.A., an indirectly, wholly owned Peruvian subsidiary of Lara Exploration Ltd. (the "Company), a wholly owned subsiduary of Quest Capital Corp.

A highly altered intrusive body lies beneath what appears to be the leached cap of a porphyry copper deposit situated on the Lara 2A and 4 mineral claims, measuring over 1 km north-south by 1.5 km east-west. An induced polarization (IP) survey conducted in 1997 yielded very encouraging results, extending the target area eastward to include a system named Mina de Socos. The expanded target area covers about 6 km^2.

Twenty-five drill holes totaling 2,876 meters have been drilled in three programs since May 1997 comprising 2,742 meters of reverse circulation and 134 meters of diamond drilling.

The author calculated a mineral inventory (classified as an *inferred resource*), of 18.6 million tonnes grading 0.53% copper, using a 0.20% copper cut-off. Within this inventory lie two higher grade blocks estimated at: 1) 6.5 million tonnes grading 0.91% copper, using a 0.50% copper cut-off; and 2) 4.8 million tonnes grading 1.04% copper using a 0.60% copper cut-off. This target zone is open to the east and west.

Significant intercepts within the target area include: 28 meters of 1.15% copper in LDD-13; 24 meters of 1.21% copper in LDD-14; 16 meters of 1.12% copper in LRC-15; 14 meters of 1.23% copper in LRC-21 and 26 meters of 0.84% copper in LRC-22. A 24 metre interval in LDD-13 and a 20 metre interval in LDD-14, diamond drill twinned holes of LRC-9A and LRC-11, respectively, significantly upgraded copper values from the reverse circulation holes by 9% and 72%. The reverse circulation drilling appears to underestimate copper grades, therefore further diamond drilling is required to verify this postulation.

Rescan Engineering completed a preliminary scoping study on the property in 1999. Their report included a mineral inventory, classified as an inferred resource, estimated at 19.7 million tonnes grading 0.47% copper using a 0.20% copper cut-off.

The Lara zone remains open to the east and west, and additional lower grade potential resource exists peripheral to the central zone. Hole LRC-3, located about 300 meters south of the central zone, yielded 54 meters grading 0.28% copper. Also, the area between Mina de Socos and the main Lara system has potential to host additional mineralization. A rock sampling program conducted west of Mina de Socos in August, 1999 yielded highly elevated copper values from bedrock identical to the leached cap found at the main Lara zone. This area lies about 800 meters east of the limit of drilling at the Lara zone.

A metallurgical study was performed in late 1998 by Plenge Laboratories, Lima, Peru on drill core samples taken from the supergene zones of holes LDD13 and LDD14. Bottle roll leach tests yielded copper extraction rates of 59.8% and 72.2%, respectively. The subsequent column leach study showed that holes LDD13 and LDD14 yielded 90.6% and 87.1% copper extract ions over 161 and 154 days, respectively, indicating that the secondary sulphides are quite amenable to SX/EW heap leach extraction methods.

The author was requested by Brian Bayley, a director in the Company, to review the documented data and to prepare an exploration program and budget that would provide the best chances of finding additional, potentially economic mineralization. In order to further test the economic potential of the Lara deposit, a combined reverse circulation and diamond drilling program is proposed. This program would explore the eastern extensions of the known mineralized body up to and including the Mina de Socos showing. Twenty-five holes, totaling 3,000 meters, would test an area that has the potential of increasing the known mineral inventory.

The cost of this program is about US$436,300, or CDN$523,560.

Introduction

The Lara property, located in coastal Peru, is owned 100% by Minas Dixon. S.A., an indirectly, wholly-owned subsidiary of Lara Exploration Ltd. (the "Company"). The Company was created as part of a plan of arrangement involving Quest Investment Corporation and a number of other companies; Lara Exploration holds the Peruvian resource assets of Quest Investment Corporation.

All work described within this report was conducted by Minas Dixon S.A. personnel except for a preliminary mapping and sampling program completed in 1994 by Villafuerte, an independant Peruvian geologist hired by Minas Dixon S.A. to assess the property.

No significant property exploration work has been done since the third drilling program completed in August, 1998. A minor amount of surface sampling was completed on the Mina de Socas zone in 1999. A column leach study was conducted by Plenge Laboratories on rejects from the mineralized zone contained in two core holes drilled in 1998. A scoping study was done by Rescan Engineering of Vancouver, B.C. in 1999.

This report is drawn from the author's own field work; a geophysical report by Arce, 1997; a preliminary scoping study conducted by Rescan Engineering, 1999; a metallurgical report on column leach tests conducted by Plenge Laboratories, Peru, 1998; various in-house reports by the author for Peruvian Gold Limited between 1995 and 1998 and a qualifying report on the property prepared for Peruvian Gold Limited in 2001.

The author performed mapping and sampling programs on the property in 1995 and 1997, supervised drilling programs in 1997 and 1998 and visited the Mina de Socos area on three separate occasions in 1999.

Disclaimer

The bulk of the data within this report was either generated by the author or was generated under his supervision. The geophysical report by Jose Arce and the report on the column leach study performed by Gustavo Plenge were both written in Peru by Peruvian nationals.

The scoping study prepared by Rescan in 1999 should have been performed by individuals who would be considered as "qualified persons" today, even though the report was commissioned prior to when the term "Qualified Person" was implemented in National Instrument 43-101.

Claims

The Lara group of claims are situated in southern coastal Peru and comprise three contiguous claims totaling 1,800 hectares (see Table 1 and Figures 2, 3, following.) The claims have not yet been legally surveyed.

COLOMBIA

ECUADOR

BRAZIL

P E R U

PACIFIC OCEAN

Piura

Chiclayo

Trujillo

Chimbote

Lima

Cuzco

BOLIVIA

LARA

① ☆

Lake Titicaca

Nazca

Puno

Arequipa

Matarani

Ilo

CHILE

81°

73°

04°

12°

0   500 Km

SCALE

LARA EXPLORATION LTD.

LARA COPPER PROJECT

FIGURE 1

Feb. 9, 2004
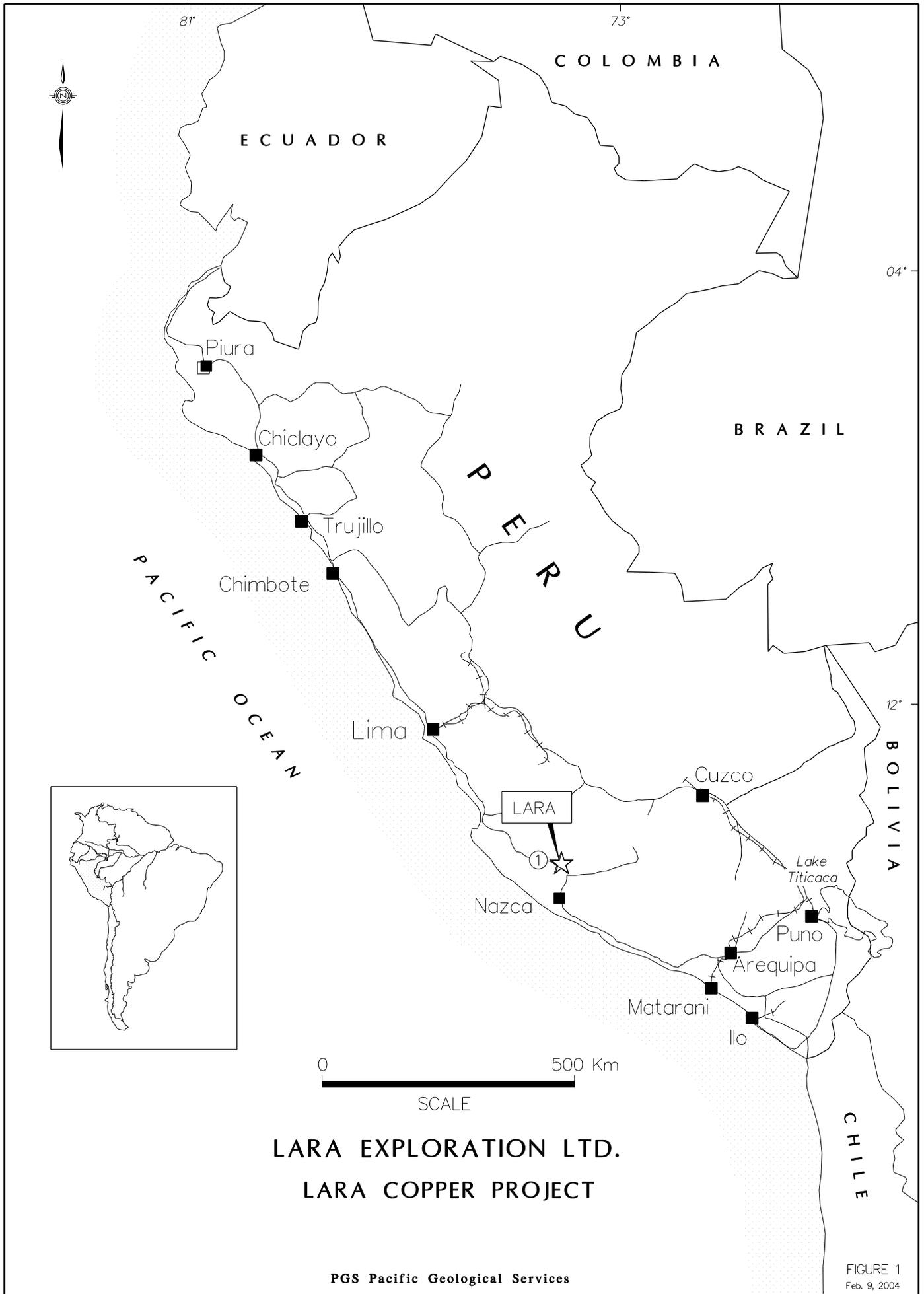
The claims are situated on topographical & geological sheet Number 29-u (1942) Laramate, first edition, 1994; 100,000 scale. The property is centered roughly at 74^0 58' west, 14^0 23' south.

The copper porphyry showings occur primarily on the Lara 4 and Lara 2A mineral claims, part of a group of three mineral claims owned by Minas Dixon, S.A., a private Peruvian company owned indirectly by Quest Investment Corporation. If the property is put into production, the Company has to pay US$500,000 to the vendor (Jaime Valdivia), either in cash or shares of the Company.

Claim staking in Peru is done by application on paper, specifying the coordinates of the claim's boundary using the country's UTM coordinate system (Peru, 1956). Claim boundaries are run on UTM grid north-south and east-west directions. The initial claim application is called a *petitorio en tramite* (petition). Once a claim is granted, it is called a *concesione* (concession); the granting process can take from one to two years.

It is required by the owner to pay US$3.00 per hectare to file the claim with the government, plus an additional administrative fee. To maintain the concession the owner pays US$3.00 per hectare per year for the first six years. If a property has not been put into production after 6 years, the owner is assessed at twice the annual rate of US$3.00.

If a property is 2,000 hectares or smaller, the owner can apply for a "small miner" status in which the annual fee is only $1.00 per hectare. A "small miner" must reapply every two years to maintain this status; the annual fees do not double after 6 years if this status is maintained (Plenge, Pers. Comm.)

Claims are not patented or unpatented, they must be applied for after staking. Mineral concessions in Peru are mapped staked. The minimum size of a claim is 100 hectares, and the maximum size is 1,000 hectares. A 1,000 hectare claim can be reduced in size (multiples of 100 hectares) subject to certain government guidelines.

The owner/Issuer holds only the mineral rights to the concessions. Surface rights are sometimes owned by farmers or other individuals if the concessions lie within a rural community. It is required (advised) to get permission from local leaders prior to commencing any work. Surface ownership is in two forms: formal title by local communities and formal title by individuals.

New laws passed in 1999 require mining companies to obtain a permit prior to commencing any drilling or major earth moving programs, such as road and drill pad construction. Depending on the amount of construction estimated, companies may be required to present an exploration program to the Ministry of Mines. Once completed, all major ground disturbances will have to be reclaimed and recontoured.

There are no known environmental liabilities that the property is subject to.

Table 1. Lara Claim Statistics

Claim	Size (hectares)	Date Requested	Code Number	Registered Owner
Lara 2A	600	Mar. 18, 1994	01-01403-94	"
Lara 4	800	June 2, 1994	01-02167-95	"
Lara 5	400	Feb. 20. 1995	01-06740-95	"

Accessibility, Climate, Local Resources, Infrastructure and Physiography

Access is via the Pan-American Highway, a distance of about 400 km southeast from Lima to the town of Palpa. From there a 40 km gravel road heads northeast to the property along the valley of Rio Viscus. The company had built an 8 km all-terrain road between Rio Viscus and the property, but much of this was washed out during the rainy season in 1999.

The terrain ranges from precipitous along the Rio Viscus valley to moderately steep and rolling hills in the vicinity of the deposit. Elevations range from about 1400 m ASL to 2000 m ASL.

Vegetation is sparse with widely spaced Peruvian and barrel cacti dominating the hillsides with a deciduous tree unfamiliar to the author. Small tufts of grass are interspersed with weeds, and groves of Molle trees (Peruvian Peppercorn) grow along the quebradas near water sources. The climate is arid, being part of the coastal desert of Peru. Precipitation occurs only in the rainy season (January-March) when electrical storms in the Sierra can cause torrential mud flows in the major rivers and creeks. Work is difficult during January and February largely because access can prohibited due to mud slides and washouts.

Water from wells should be feasible due to water encountered in at least one drill hole located in a dry creek bed near the center of the property. No electrical power is available; the nearest source of electricity is in the town of Palpa.

The town of Nazca, 45 km southeast from Palpa, has sufficient infrastructure and supplies to be used as a base of operations, and Palpa has labour and minor amenities.

There appear to be sufficient piedmonts, along the flanks of the principle quebraba draining the property, to be able to support leach pads and waste dump sites.

The author is not conversant on overlapping or coinciding surface and sub-surface rights in Peru. There is, however, sufficient mineral claim coverage to secure access and development of the property should that come about.

LEGEND

CLAIM	HECTARES	STATUS
LARA 2A	600	TITLED
LARA 4	800	TITLED
LARA 5	400	TITLED

AREA OF ALTERED AND MINERALIZED PORPHYRY, AND HIGH IP CHARGEABILITY

14° 20' S

LARA 2A

Mina de Socos

LARA 4

LARA 5

Mina Lambrasnivoc

0   1.0   2.0   3.0   4.0 KM

14° 30' S
75° 00' W

FIGURE2.GCD

LARA EXPLORATION LTD.

LARA PROPERTY, PERU

CLAIM LOCATIONS

SCALE	DATE	DRAWN BY	FIGURE
1:100,000	Feb. 9, 2004	JN	2
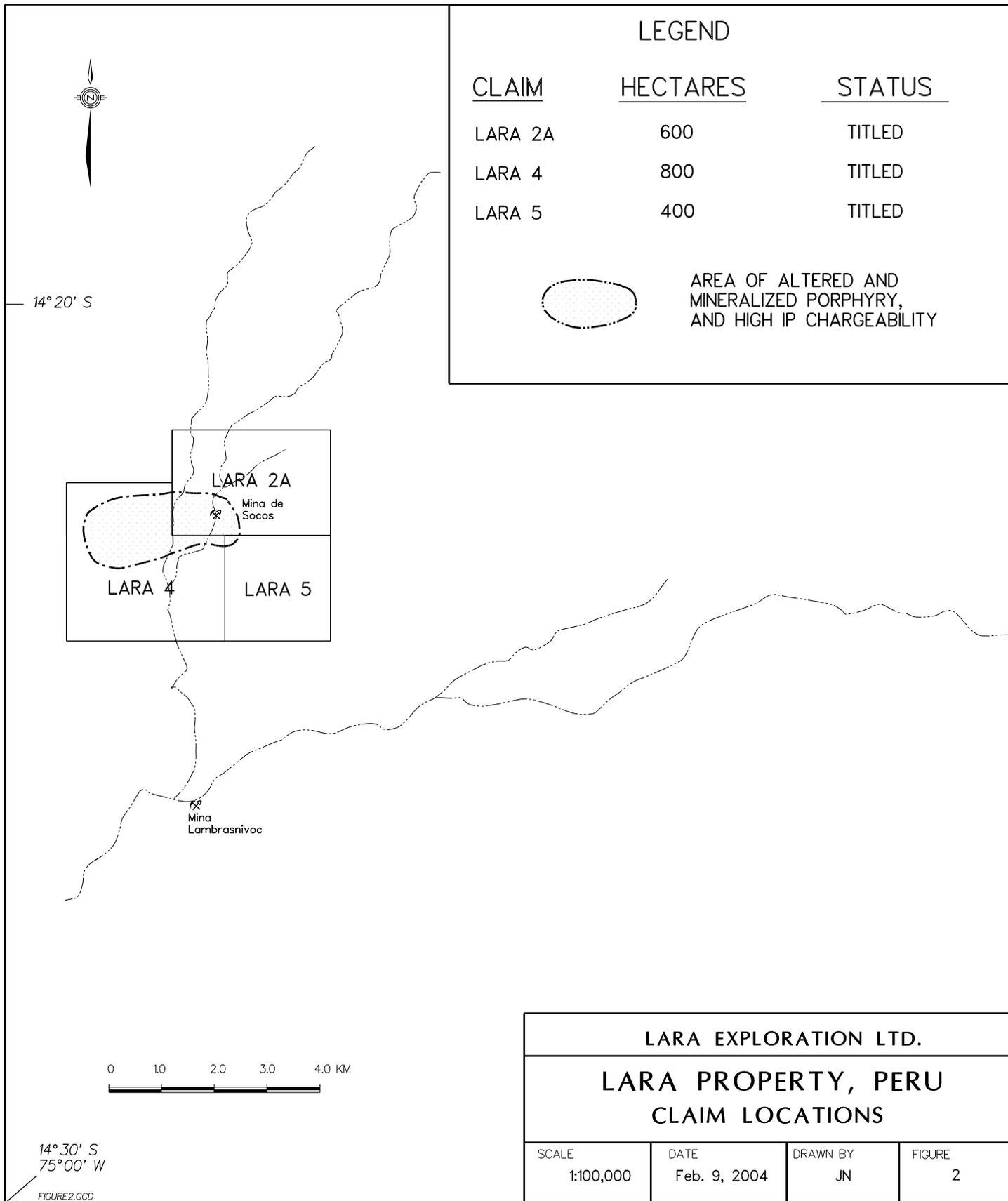
History

The author has not made an extensive search into the mining and/or exploration history of this district. A 100,000 scale geology map shows one old mines on the property: *Mina de Socos* on Lara 2A claim. It is the author's understanding that *Mina de Socos* contains primarily copper mineralization, but it is likely that gold may have been of considerable interest.

In 1989, Jaime Valdivia, a geologist with Centromin, a State Peruvian mining company, while exploring for gold deposits, examined the *Mina de Socos* mineral occurrence and noted the regional geological setting. In early 1994, Sr. Valdivia met with the president of Minas Dixon S.A. and discussed the possibility of the *Mina de Socos* area being prospective for a porphyry copper deposit. Minas Dixon S.A. immediately staked claims in the area and instigated its first geological reconnaissance mapping and sampling programs. The programs confirmed the existence of a porphyry copper target (Villafuerte, 1994.)

Other than the small copper in quartz vein at *Mina de Socos*, probably mined by "Informales", no record or evidence exists of anyone having conducted exploration or exploitation work on the ground now recognized as being a porphyry copper target. No records exist of there having been any prior mineral claims staked over the Lara property.

Numerous small active mining operations were observed on the road between Lara and the community of Palpa. Narrow gold-bearing quartz veins, hosted by massive granodiorite of the Coastal Batholith, are being exploited.

Subsequent to the mapping and sampling project conducted by Villafuerte in 1994, the property was visited by Company personnel and the property vendor (Valdivia) in early 1995. The Company then commissioned the author to perform a detailed mapping and sampling program to further assess the property in 1995.

An induced polarization sounding survey, employing the Schlumberger method, was completed in early 1997. Subsequently, about 8 km of access roads and drill platforms were built in April and May 1997.

A five-hole, reverse circulation drilling program was conducted in May 1997. Following the discovery of a chalcocite-rich, supergene horizon in the last two holes, additional drilling was done in two subsequent programs in October 1997 and August 1998. In the three programs a total of 2,742 meters of reverse circulation and 134 meters of core were drilled.

In 1999, Rescan Engineering calculated an inferred resource of 19.7 million tonnes grading 0.47% copper, using a 0.20% copper cut-off. The author believes this estimate to be relevant and accurate given the data provided and methodology used.

Regional Geology & Geomorphology

The claims are situated within the Coastal Batholith which extends for at least 800 km NW-SE and is about 80 km wide. Copper deposits contained within this belt include the Toquepala, Cuajone, Quellaveco and Cerro Verde porphyry deposits in the southeast, and the manto, volcanic and vein copper deposits near Lima in the northwest. The Lara property is located roughly in the central part of the batholith, and the nearest copper porphyry is El Puquio, located about 70 km to the NW.

The late Cretaceous to early Tertiary Coastal Batholith occupies the central part of the district, consisting primarily of granodiorite and tonalite but containing phases ranging from diorite to granite. The Coastal Batholith was emplaced during the "Peruvian Phase" of the mid-Cretaceous Andean Orogeny.

The batholith intruded metasedimentary rocks of the Jurassic-Cretaceous Yura Group; quartzite seems to be the dominant lithology.

A series of small Tertiary plutons intrude the Coastal Batholith. They are mapped bysome as granites, but the author's observations suggest an aplite to rhyolite porphyry classification may be more appropriate for some. Dykes of andesitic and dacitic composition transect both the Coastal Batholith and the younger felsic intrusions.

The youngest lithologies in the area belong to the late Tertiary Nazca Group. They consist of varicoloured sub-aerial volcanic flows, agglomerates, breccias and tuff. These rocks appear unaltered and seem to postdate the porphyry copper intrusion/alteration event. They are of minor importance in the area of the Lara claims but are prevalent in higher elevations north and east of the property.

The regional geology map shows few structures. A series of NW-SE trending block faults traverse the district, in places showing relative displacements between the above-mentioned lithologies. One fault, about 20 km east of Lara, is shown trending NNE-SSW along Rio de Tomate. Minor NW-SE trending fold axes are shown to occur within the Nazca volcanics.

Climatic changes over periods of millennia and longer has resulted in deep weathering of bedrock, which is particularly evident in the batholith. Heavy boulder-clay colluvium is ubiquitous and periodically has been transported as gravity slides. Sections through this material in the larger quebradas show colluvial material interlayered with alluvium, ranging from quiescent, thinly layered silt and sand laminae to large cobble and boulder strewn channels.

The rainy season is from December to March, at which time the quebradas are filled with water. Periods of exceptional precipitation incise the colluvium, locally exposing the regolith and underlying bedrock.

Property Geology

The main area of the Lara prospect was mapped and sampled by the author in 1995; the area around Mina de Socos, east of the main Lara target, was mapped by the author in May, 1997. The details of the geology, geochemistry and drill sites are presented on Map 1 found in the back of this report; a compilation of the geology and IP survey is presented in Figure 4, following.

Lara Zone
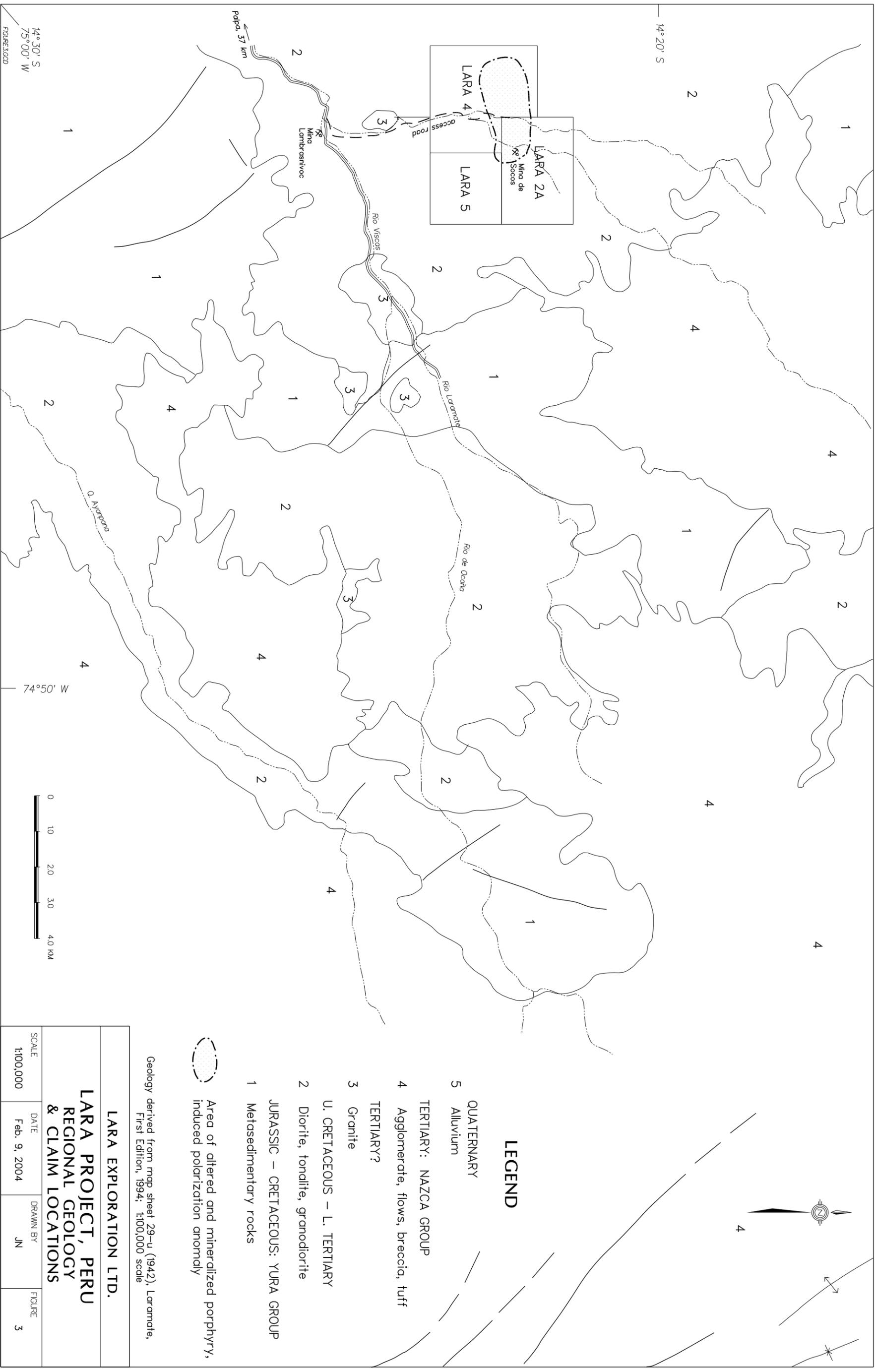**Lithologies & Alteration**

The southern and southwestern portions of the Lara property are underlain by hornblende diorite. The rock is medium grained, light to medium gray, and contains minor potash feldspar porphyry; locally the rock grades to monzonite composition. The diorite is fairly fresh in appearance but grades into a propylitized phase containing epidote, chlorite, calcite and saussaurite along fractures. Transitional contacts between "fresh," propylitized and other phases are somewhat arbitrary in places, but most of the contacts seem to be fault related, as observed in numerousfault slips in the more competent rock units along the southern and southwestern margins of the target area.

The unaltered and propylitic phases of the diorite change rapidly northwards to an intensely argillic altered rock. The margins of the argillic altered phase exhibits parallel sheeting along the
lower parts of *Qda. Socos* and *Qda. Ayjaracancha* and in a few locations along the western margin of the porphyry. The sheeting in the former location trends about AZ.165/85NE to vertical dip and about AZ.045/vert. dip in the latter. Fracture densities range from 20-40/metre to 50-150/meter in these areas, respectively. Jarosite is the dominant limonite present, as well as minor to moderate amounts of iron sulphates and gypsum. This assemblage is typical of a leached "pyritic halo" in a porphyry copper deposit.

North and east from these respective sites the argillic alteration intensifies, eventually grading into the phyllic aureole. The unidirectional jointing is no longer evident but is replaced by a rhombohedral fracture pattern. Goethite is roughly equal to jarosite in concentration, locally exceeding it; and hematite occurs randomly throughout it, but generally increasing in intensity towards the center of the system. Tenorite/neotocite is seen locally with concentrations of goethite.

Quartz veins become noticeable roughly midway between the pyritic and sericitic (phyllic) halos, becoming more common towards the north (porphyry center). Veins are usually a few mm to cm wide, and no veins were observed exceeding about 5 cm to 10 cm across.

An area of recessive weathering, sericitic aplite/quartz monzonite outcrops in *Qba. Ayjaracancha* just north of an east-west trending dacite dyke; this dyke probably occupies a fault

14°20' S

14°30' S
75°00' W

74°50' W

FIGURE3.GCD

LARA 4

LARA 2A

LARA 5

Mina de
Socos

access road

Mina
Lambrasnivoc

Palpa, 37 km

Río Viscas

Río Laramate

Río de Ocaña

Q. Ayarqana

0   10   20   30   4.0 KM

LEGEND

5   QUATERNARY
Alluvium

TERTIARY: NAZCA GROUP

4   Agglomerate, flows, breccia, tuff

TERTIARY?

3   Granite

U. CRETACEOUS – L. TERTIARY

2   Diorite, tonalite, granodiorite

JURASSIC – CRETACEOUS: YURA GROUP

1   Metasedimentary rocks

Area of altered and mineralized porphyry,
induced polarization anomaly

Geology derived from map sheet 29–u (1942), Laramate,
First Edition, 1994; 1:100,000 scale

IP CHARGEABILITY CONTOURS
SHOWING mV/VOLT VALUES

N

LARA 2A

LARA 4

Section SW-NE (figure 7)

LARA 5
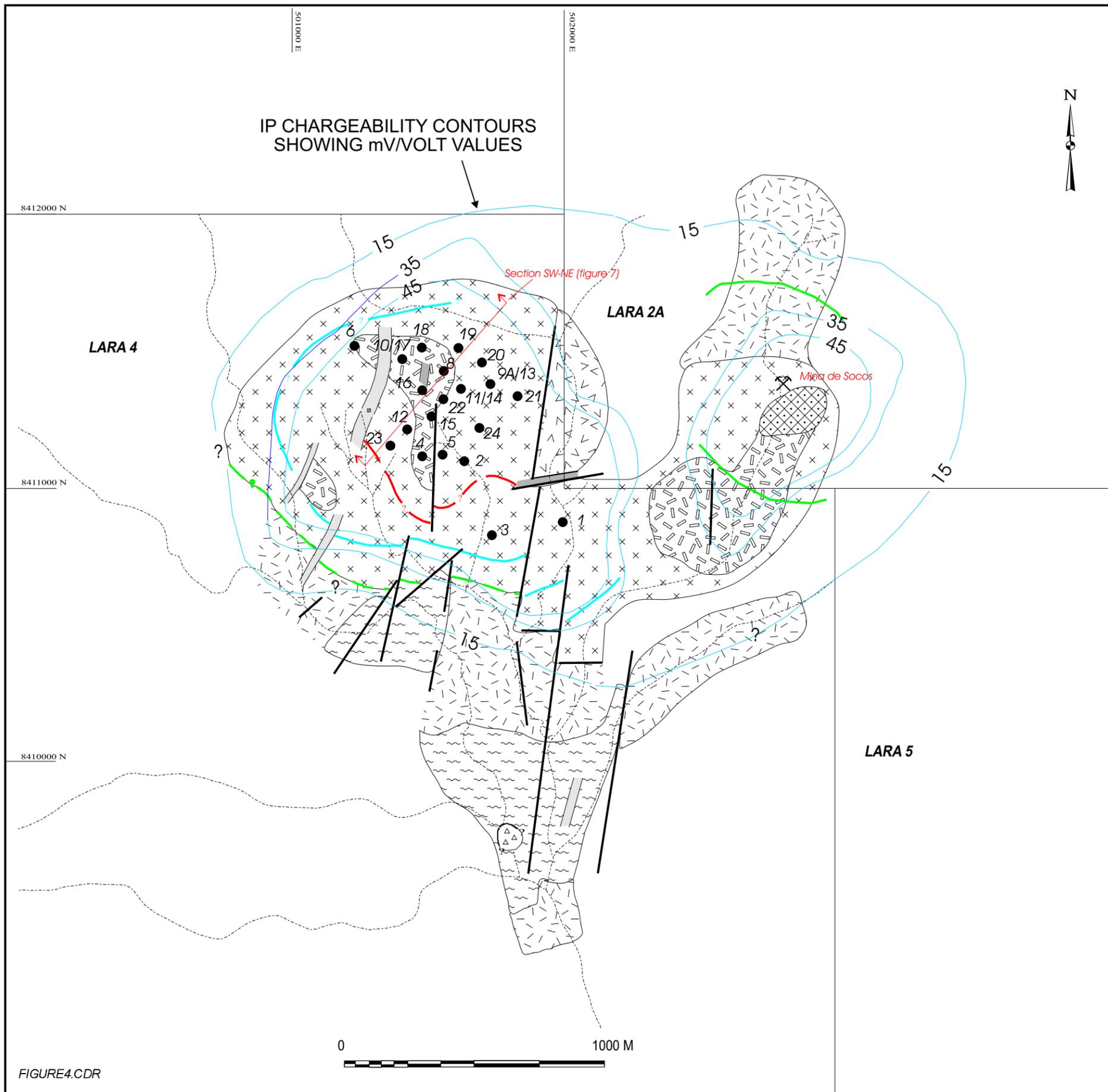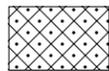
DACITE PORPHYRY

BRECCIA PIPE

APLITE DYKES

ANDESITE DYKES

QUARTZ MONZONITE/APLITE/
GRANITE PHASE, VEINED WITH
QUARTZ

PHYLLIC AND POTASSIC
ALTERED QUARTZ MONZONITE,
AND APLITE

ARGILLIC ALTERED PORPHYRY
(LARGELY DIORITE)
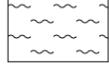
PROPYLITIZED DIORITE

UNALTERED DIORITE

FAULT

OUTER LIMIT OF POTASSIC-
PHYLLIC ALTERATION HALO

INNER LIMIT OF PYRITIC
ALTERATION HALO
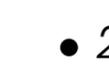
INNER LIMIT OF PROPYLITIC
ALTERATION HALO

● 2   R.C. DRILL HOLE

SECTION LINE

LARA EXPLORATION LTD.

LARA PORPHYRY COPPER PROJECT
WESTERN PERU
GENERALIZED GEOLOGY

0   1000 M

FIGURE4.CDR

FEB. 9, 2004   FIGURE 4

-12-

along the same trend. The aplite/quartz monzonite contains up to 10% 1mm diameter quartz eyes. Sericitic alteration is common in this unit, and minor secondary biotite is also present. Quartz and goethite veins are present but not as plentiful as in the argillic phase to the south. This outcrop area also contains some diorite, but no distinct contacts were observed.

A small outcrop of medium grained quartz monzonite occurs about 200 meters north of the above area. Malachite is seen here filling interstices in colluvium above the outcrop; this occurence is probably a precipitation from an outflow from a preexisting chalcocite blanket in response to changing Eh-pH and groundwater conditions (Brooks, pers. comm.) Malachite also coats fractures in the outcrop, which may also be derived from the outflow; however, small rosettes of pitch limonite (= to goethite?) are found in the fractures suggesting that this rock may have contained primary chalcopyrite even if the malachite is not derived from it.

On the summit midway between *Qba. Ayjaracancha* and *Qba. Jayacyana* occurs a fine to medium grained quartz-eye porphyry. This unit is best described as an aplite or rhyolite porphyry due to a lack of a crystalline matrix in most places; but locally distinct feldspar crystals are present and a classification of quartz monzonite or granite would be appropriate. This unit is crosscut by numerous quartz veins up to a few cm across. The veins locally form stockworks but there is also a dominant, unidirectional set trending north-south and dipping 65 degrees east.

Jarosite and goethite is not as common as in the argillic altered phases surrounding the summit, but hematite is much more prevalent, in places up to 40% of the total limonite content.

The aplite/quartz porphyry unit seems to occupy the central core of the intrusive complex; it is clearly the youngest phase of the porphyry and is much more saturated than the peripheral phases. This could represent a silica cap, or the late stage barren core to a porphyry copper system.

Andesite porphyry and light coloured felsite (dacite) dykes traverse the porphyry system. It appears that the felsic dykes are the youngest of the two, and both types are post-mineral. They have not been altered like the diorite or aplite, although some limited argillic alteration does occur in the andesite dykes where they are cut by faults. Copper carbonates and tenorite/neotocite are common in fractures in the dacite dykes, and locally in the andesite. This does not appear to be caused by primary copper sulphides within the dykes but rather by a scavenging affect from the surrounding mineralized porphyry they intrude.

Structure

Block faulting is the dominant structural feature on the Lara property. Three major trends are recorded, and their relative frequency of occurrence and significance, in decreasing order, appear to be: 1) approximately north-south (AZ. 010) with near vertical dips; 2) roughly east-west strikes with steep northerly to vertical dips and 3) NE-SW trending strikes (AZ. 060 is common) with steep northwesterly dips. The north-south faults parallel the direction of most of

the creeks (quebradas) in the area, and many of the bends in the creeks can be attributed to one of the other fault sets. Both dyke units are found in all three fault trends, but the north-south set is the dominant host structure.

There is an apparent right lateral displacement along the north-south faults, in the order of 100 m + , but a true sense of vertical displacement is not clear. The joint sets in the pyritic halo are very steep to vertical along the SE and SW margins of the porphyry. This would indicate that they are situated along the periphery of the system at a level <u>below</u> the dome or "cap" of the porphyry.

An interesting observation is the lack of any evidence for the NW-SE fault trend shown on the regional geology map. One would expect to see it represented in some form of fault slip, but none was recorded.

The porphyry system at Lara is at least 1 km across north-south and possibly up to 1.5 km across east-west. The report by Villafuerte (1994) suggests that the system may be as large as 2 km east-west, the IP survey and author's mapping in 1997 support this interpretation. A concentric zone of typical porphyry alteration envelopes is preserved in the southwestern and southern portions of the system, but the eastern and southeastern parts of the porphyry have been dissected by the aforementioned faults, offsetting them slightly southwards and complicating interpretation somewhat. In any event, there appears to be a copper porphyry system underlying the Lara 2A and Lara 4 claims with an ovoid shape at least 1 km north-south by 1.5 km east-west.

Mineralization & Geochemistry

The Lara 2Aand 4 claims were examined by Sr. Villafuerte on two occasions in 1994 and 1995. During these visits he collected ninety-one rock samples from various locations on Lara 2A and Lara 4. His sampling extended about 1000 m west and 1500 m east of the area described within this report. Sixty-one of his samples lie within the map boundary of this report, and at least one-half of these were examined during mapping. The author collected fifteen samples from various sites on Lara 4 in 1995 and five samples from Lara 2A and 4 in 1997 (see Map 2, in pocket.) All samples collected in 1995 were analyzed for Cu and Au, and fifty-six samples collected by Villafuerte were also analyzed for Ag, Pb, Zn, As and Sb. The five samples taken in 1997 were analyzed for gold using fire assay-atomic absorption finish and for multi-elements using ICP.

One of the objectives of the author's mapping/sampling program was to endeavour to identify the phases of a porphyry system within the leached cap and to try to estimate the grade and mineralogy of the system based on geochemical sampling and recognition of limonites. Years of research and field applications, particularly by Kennecott geologists, showed that the ratio of jarosite to goethite multiplied by the geochemical assay for Cu would yield a fair approximation of the grade of the primary sulphides prior to leaching.

Copper values within the map area range from a low of 57 ppm to a high of 23,100 ppm. Malachite was observed at some of the sites yielding highly anomalous copper values (+/- >2000 ppm). The area between the central core of the porphyry and *Qda. Ayjaracancha* to the east contains many occurrences with malachite and tenorite/neotocite. The 23,100 ppm value came from the colluvium laced with malachite, thought to be a possible outflow from a supergene enrichment zone. Samples collected by Villafuerte from the felsic dykes also show highly elevated copper values, again, this is due to the presence of copper carbonates and tenorite/neotocite.

Within the areas mapped as the "pyritic halo" values ranged from 92 ppm to 662 ppm Cu. The one exception was at the site of samples #017 and #2269. The rock here is coated with iron sulphates and randomly veined with quartz-goethite veins often coated with neotocite/tenorite and minor malachite. Sample #017 assayed 3370 ppm Cu. I tried to avoid including these veins in sample #2269, yet it still yielded a value of 2330 ppm Cu. A manganiferous wad (caliche) occurs downstream from here in the creek bed for about 50 m to 100 m. This material was not sampled, but it is likely that it would yield elevated copper values.

The argillic to phyllic aureoles contain more goethite relative to jarosite (chalcopyrite and pyrite as primary sulphides, respectively.) Copper values range from 288 ppm to 1560 ppm, and an average of 600 ppm to 800 ppm is indicated. Goethite and hematite contents tend to increase towards the core of the porphyry as observed in the three quebradas that drain it; quartz, sericite and secondary biotite follow the same pattern.

Samples collected from the aplitic core tend to contain a little less copper; values range from 109 ppm to 501 ppm. The 4 samples collected by the author from the aplite averaged 175 ppm Cu.

The estimated values of the primary sulphides are documented on Map 3 of the author's 1995 report but are not shown on Map 2 of the current report. Estimates were made only from samples collected by the author and the sites of the previous sampling that were visited. All previous sites that contained copper carbonates and/or neotocite were excluded from the estimation.

Values within the pyritic halo range from 800 ppm to 3500 ppm Cu. Two exceptions are the samples cited earlier where tenorite/neotocite and minor malachite were observed in quartz-goethite veins. These samples yielded estimated primary sulphide grades of 5429 ppm and 13,480 ppm Cu, but they probably contain other copper minerals biasing the values.

Within the argillic/phyllic zones the estimated primary sulphide grades range from 750 ppm to 2750 ppm. There is not sufficient sampling done within this zone to give a clear pattern of mineral zonation at this time.

Samples from the silicic core (aplite) do not reveal much as there is little limonite found within it--mostly hematite. If the aplite represents the "barren" silicic-potassic core of a porphyry system, then one would not expect highly anomalous values within it.

Hematite is present mainly as veinlets and fracture coatings interspersed with the other limonites. No zones consisting strictly of hematite were observed in the argillic, phyllic or pyritic aureoles that might represent the weathering effect of a preexisting chalcocite blanket. When hematite consists of less than 50% of the total limonite, it is difficult to ascertain if a "re-leached" chalcocite blanket exists; however, this does not preclude the existence of an unleached chalcocite blanket on the Lara porphyry system (Brooks, pers. comm.) The most compelling evidence for the presence of a chalcocite enrichment blanket is the malachite "outflow" found in the colluvium in *Qda. Ayjaracancha.* The abundance of malachite in showings on the slope between the summit and the quebrada to the east of it might indicate that a zone of supergene enrichment may underlie this slope. A similar target could be found along the western and southwestern portions of the system as well.

Gold and silver do not seem to be highly elevated in this porphyry; only a few samples ran greater than 100 ppb Au. The most significant samples are 132 and 133, taken near or within an andesite dyke about 100 m SW of the summit. These samples also ran 31 ppm Ag, 35 ppm Sb, 2640 ppm Cu and 13 ppm Ag, 35 ppm Sb, 6015 ppm Cu, respectively. I did not visit this site, but because of its location near a dyke-fault? contact, and the presence of elevated Sb, I suspect that this is caused by some minerals not necessarily related to the porphyry.

Mina de Socos Zone

This area was mapped in 1997 to in-fill the geology along *Qba. Mina de Socos*. An induced polarization sounding survey was performed on the Lara prospect early in 1997 and indicated that the Lara porphyry system may extend to Mina de Socos, or else a smaller, secondary target may exist here. More will be discussed on the induced polarization survey in a later section.

Cliff-forming outcrops occur along *Qba. Mina de Socos*, 1 to 1.5 km east of the center of the Lara system. This rock is the same quartz eye rhyolite/aplite that occurs on the ridge crests and summits to the west. Locally the rock is coarse grained and could be classified as a true granite. The rock here is fairly massive, fresh and contains few quartz veins. Within 200 meters of the bend in the creek (heading north) the rock becomes quite shattered and coated with limonites. Pyrite becomes visible as well as some malachite. Argillic alteration becomes more intense heading north, and some parallel quartz veins start to appear.

A medium to coarse grained diorite is in contact with the granitic unit along an apparent east-west fault. The rock is much fresher than the granite and contains pyrite and lesser chalcopyrite along parallel fractures that strike 100^0 azimuth and dip 80^0 north. The diorite becomes more altered and fractured towards the north, containing more copper oxides, and sulphides in general. The diorite is exposed over about 50 meters in the creek and is terminated

top the north by a large quartz vein that may be up to 5 m thick. The vein is coated with a thin veneer of jarosite; pyrite was seen on fresh surfaces.

Immediately past the quartz occurs a fairly massive, gray to black porphyritic dacite intrusive. The rock is innocuous in appearance, containing little sign of oxidation in the creek bed but showing limonite and iron sulphates along fractures above the water table. It contains disseminated and fracture filled pyrite and chalcopyrite throughout its extent at an estimated ratio of 4:1. The total copper grade is probably not over 0.2%; two chip samples collected from this unit (#'s 73544, 73545) ran 1094 and 938 ppm Cu, respectively.

Two large quartz veins, each about 1 meter wide, trend roughly north-south with a vertical dip within the dacite near its northern margin. Two large pits occurring in a gully that crosscuts these veins appear to be at least in part man-made, and numerous other pits and quartz vein stockpiles occur on the piedmont west of here. Malachite and tenorite are common in quartz boulders stockpiled near the workings.

The dacite unit is exposed over about 100+ meters in the creek and is truncated by another "fresh" coarse grained diorite dyke to the north. The dyke trends roughly NE-SW and separates the dacite from moderately argillic altered and sulphidized diorite to the north. Total sulphide content is in the order of 2%. An east-west, vertically dipping, 1 meter wide fault cross cuts the diorite; malachite is common in the fault zone.

The diorite becomes fairly fresh again about 200 meters north of this outcrop, containing up to 10% pyrite along fractures and as disseminations. The biotites are relatively fresh in appearance as well. This appears to be the northern extent of the pyrite halo formed by the Mina de Socos system. The next outcrops, about 75 to 100 meters northwest, are very fresh and contain virtually no sulphides. Some epidote and chlorite is present, suggestive of weak propylitic alteration. In addition, the composition of the rock has changed somewhat, appearing more potassic like a monzonite, but some diorite is still evident.

A large, post-mineral dacite dyke outcrops roughly 200 meters east of Mina de Socos. The porphyry in contact with, and immediately west of the dyke is intensely altered, similar to that seen in the main Lara zone 800+ meters to the west. This alteration is much more intense than the alteration halo seen around the Socos system and could not have been caused by it. The area was re-examined by the author in 1999, accompanied by D.A. Henstridge, President, Peruvian Gold Ltd. and Ruben Tejada, senior geologist, Minas Dixon, S.A. The collective opinion was that this alteration could not have been caused by the weak Socos dacite porphyry and that this area may represent the eastern extremity of the Lara system, bounded by a large north-south fault subsequently occupied by the dacite dyke.

A program of mapping and rock sampling was performed in August 1999. The results of this work yielded anomalous copper values over an area 300 meters north-south by 150 meters east-west with values ranging from 300 ppm to 800 ppm copper. These highly elevated copper

values, in rocks identical to the leached capping found overlying the resource already drilled on Lara, support the earlier interpretation that the Lara porphyry system extends from the known resource eastward to Mina de Socos, a distance of 800 meters. The copper anomaly also coincides with an induced polarization anomaly discovered in the 1997 geophysical survey. The untested area between Lara and Mina de Socos has the *potential* of significantly increasing the existing resource.

Induced Polarization Survey

A reconnaissance IP survey was performed early in 1997. Jose Arce specializes in using the sounding technique and has demonstrated its effectiveness in 52 porphyry deposits throughout Peru. Sixty-two stations were employed in this survey, and the details of the survey parameters are discussed in a report by Arce (February, 1997).

Arce presents a coloured chargeability plan using five threshold levels: background (<15 mV/V), weak anomaly (15-25 mV/V), medium intensity (25-35 mV/V), high chargeability (35-45 mV/V) and strong anomaly (>45 mV/V.) Contours derived from this data are presented in Figure 4. Theoretically, any values greater than 150% of background (15 mV/V) are considered significant for prospecting. The limits of the weakly anomalous values cover an area of 6 km^2 and the highly anomalous values, centered over the main Lara target and Mina de Socos cover 1 km^2 and 0.25 km^2, respectively. What is interesting is how the 35 mV/V contour nearly coincides with the pyritic halo as mapped by the author in 1995; the Mina de Socos system is similarly outlined.

A detailed description of the survey results will not be discussed here, but an example provided by Arce, and considered fairly representative of all other soundings on Lara, will be mentioned. At sounding station 0, located at the topographic summit, and interpreted "center" of the Lara system, the following observations are made:

Resisitivity: R1. 50 ohm-metres from 0 meters to 9 meters of depth.
                       R2. 130 ohm-metres from 9 meters to 40 meters of depth.
                       R3. 42 ohm-metres from 40 meters to >200 meters of depth.
Chargeability: M1. Background of 2 mV/V from 0 to 68 meters of depth.
                       M2. Strong anomaly, 65 mV/V, from 68 meters to >200 meters of depth.

Arce points out that the high chargeability at this station (65 mV/V) could represent more than 10% total metallic sulphides per volume.

All the geological mapping and geochemical surveys documented within this report were conducted by technical staff or consultants directly employed by the Company or its affiliate Minas Dixon S.A. Only the induced polarization survey was performed by an outside consultant, Jose Arce. There is no evidence of any significant discrepencies in the results obtained in the surveys described above. Two of the rock samples collected by the author produced higher than

usual estimated primary copper values, probably due to the presence of manganese minerals in these samples that acted as scavengers and thus concentrated anomalous amounts of copper.

The induced polarization survey yielded a pattern of chargeability anomalies that almost exactly coincides with the geological/alteration/mineralization boundaries mapped by the author in 1995. The IP survey was conducted in 1997, and as such, had no influence the author's interpretations. No opinion is offered on the quality of the IP data within the bounds of the anomalies.

Drilling Programs

Five reverse circulation (RC) holes totaling 995 meters were drilled in May 1997. The sites were selected based on the results of the IP survey in conjunction with the known geology, but some of the proposed sites had to be modified slightly because the bulldozer was not able to access all the areas due to continuous break-downs. The discovery of significant amounts of chalcocite in holes LRC-4 and LRC-5 prompted an additional seven-hole program, totaling 709 meters, to test the central portion of the porphyry north of holes LRC-4 and LRC-5. The second drilling program was conducted in October 1997. The third program consisted of nine reverse circulation and three combined reverse circulation/diamond drill holes totaling 1038 meters and 134 meters, respectively. The table below summarizes the drilling statistics.

Table 2. Drilling Statistics

Hole no.	Easting	Northing	Elev.	Azimuth	Dip	Length (m)	best Intercept	from	to	true thickness*
LRC-1	501993	8410883	1611	360	-90	137	NA	NA	NA	NA
LRC-2	501635	8411105	1719	360	-90	212		0	68	68
LRC-3	501738	8410836	1651	360	-90	168	NA	NA	NA	NA
LRC-4	501481	8411120	1767	360	-90	222	0.54	28	70	42
LRC-5	501554	8411129	1727	325	-60	256	0.56	18	38	20
LRC-6	501237	8411524	1860	278	-50	100	NA	NA	NA	NA
LRC-7	501529	8411324	1847	145	-60	21	NA	NA	NA	NA
LRC-8	501562	8411432	1809	360	-90	100	0.48	42	50	8
LRC-9A/LDD-13	501732	8411382	1779	360	-90	98/110.6	0.33/0.95	14/74	16/110.6	2/36.6
LRC-10/LDD-17	501405	8411476	1865	360	-90	100/56.1	0.51/NA	62/NA	86/NA	24/NA
LRC-11/LDD-14	501621	8411368	1820	360	-90	92/108.4	0.29/1.08	52/69	58/97	6/28
LRC-12	501423	8411221	1783	360	-90	100	0.51	36	100	64
LRC-15	501511	8411264	1808	360	-90	102	0.61	58	102	44
LRC-16	501485	8411363	1858	360	-90	100	0.45	36	46	10
LRC-18	501483	8411523	1811	360	-90	90	NA	NA	NA	NA
LRC-19	501611	8411515	1751	360	-90	96	0.59	36	52	16
LRC-20	501702	8411463	1750	360	-90	96	0.35	22	38	16
LRC-21	501824	8411334	1754	360	-90	114	0.74	78	114	36
LRC-22	501555	8411326	1844	360	-90	120	0.68	84	120	36
LRC-23	501365	8411161	1730	360	-90	90	0.38	26	94	64

| LRC-24 | 501692 | 8411221 | 1741 | 360 | -90 | 90 | 0.42 | 73 | 86 | 13 |

* Drill intercepts were sufficiently perpendicular to the gently dipping supergene horizon to state that the intercept drilled is almost the true thickness (see Figures 5 to 7 for reference.)

Drill holes 1, 3, 6, 18, 19 are located within the pyritic halo, while the remaining holes are situated within the phyllic-potassic halos.

It was observed that much of the area was hosted by rock of similar texture, though compositionally there may have been a difference between the barren rocks in the propylitic halo and the potash enriched phase(s) near the core of the system. For example, in the creek in which hole LRC-1 was drilled (see figure 4 and Map 1), one passes from a fresh looking to slightly propylitized diorite into the "pyrite halo" which appears to be the same host rock, except for the strong parallel sheeting and jarosite and pyrite alteration imparted on it. Further up the creek the rock becomes more intensely kaolinized, friable, and geothite becomes the dominant limonite along rhombohedral fracture sets rather than parallel ones. The rock may be a little more potassic, say monzonite rather than diorite, but whether this is a primary or secondary feature is not certain. Secondary biotite is observed in this same unit towards the center of the Lara system, yet the rock looks not dissimilar to that seen previously. The quartz monzonite and aplite/quartz porphyry seen in the creek north of hole LRC-1 is clearly a different unit, owing to the presence of quite visible quartz phenocrysts throughout the matrix; this unit has undergone potassic alteration (sericite and biotite) and is recessive weathering, different from the rhyolite/aplite/granite unit seen near the center of the Lara system and south of Mina de Socos. A brief synopsis of each hole follows:

LRC-1

Alluvial overburden was encountered to 27 meters followed by a contiguous section of diorite/monzonite (classified as 'granodiorite' by the field geologist.) The rock is chloritized and contains from 5% to 15% disseminated pyrite. Minor specks of chalcopyrite were observed in the fine fraction between 54 and 56 meters. Quartz veining is present but constitutes no more than 5% of rock, chloritization associated with quartz and appears to increase with depth. Minor epidote and hematite appear at about 70 meters depth. Traces of chalcopyrite are seen in the heavy, panned fraction at 124-130 meters and at 134-136 meters. A dark, soft, sooty mineral observed in upper portion of hole might be chalcocite.

LRC-2

This hole was classified as granodiorite throughout. Some malachite seen from surface to about 24 meters where pyrite and some chalcopyrite is visible. Chlorite, epidote and some magnetite observed from surface, possibly some chalcocite at 10 - 12 meters. Colour change from brown to gray at 46 meters--depth of weathering? Malachite, chrysocolla, azurite, chalcocite? and covellite? become noticeable between 48 and 60 meters. The observations in this interval agree with the assay results (see cross-section.) Rock becomes whiter in colour and copper oxides

disappear at 70 meters, but no mention of lithology change. Pyrite content increases as does chlorite and magnetite. Sericite first noted at 134 meters. Rock colour changes from light to gray throughout remainder of hole.

LRC-3

The rock is very broken and possibly mixed with colluvium for the first few meters. Oxidized with jarosite and limonites, traces of sericite, increasing with depth. Described as "altered diorite" throughout the hole. Traces of magnetite and epidote. Sulphides first encountered at 60 meters, mostly pyrite (75% to 90% pyrite--10% to 25% chalcopyrite), total sulphide content ranges from 0.5% to 3%. Rock is classified as "fresh" rather than "altered" from this point on--possibly weathering effect. Some signs of chalcocite? between 60 and 80 meters. Some signs of molybdenite were mentioned between 146 and 158 meters.

LRC-4

Rock is described as diorite near surface having a maroon colour, probably hematite which is common on nearby outcrops. Chrysocolla and goethite noted starting at about 14 meters. Oxidation extends to about 28 meters depth after which it has a gray colour. Some signs of copper oxides continue, as well as a black mineral described as manganese. Increased silicification noted at 62 meters, accompanied by geothite, chrysocolla and an unidentified black mineral (chalcocite?) Classification changed from diorite to monzonite after 70 meters depth. Some boxwork geothite after pyrite noted, sulphide content is decreasing to about 1% level, or less, sericite is increasing. Rock changes to granodiorite (increased quartz?) after 128 meters; sulphides and copper oxides increase as well--concurs with assays and section. Described as containing biotite, quartz and hornblende and disseminations of sulphides (pyrite>chalcopyrite.) Sulphide content increases hereafter, up to 7% estimated. Traces of secondary biotite seen at 202 meters. A granitic phase (aplite unit?) was encountered at 213 meters; contains quartz, potash feldspar and boxworks after pyrite. The sulphide content drops off dramatically and mafics are minor. It is likely that the "monzonite" is in fact an andesite dyke and the "granite" is the late stage aplite/rhyolite/granite unit. Both these units would be expected to be lower in copper grades. The "granodiorite" may also be equivalent to the diorite/monzonite phase logged at the top of this hole and in the other holes. A clear differentiation is not stated; the drill chips and outcrops observed by the author along the drill sites of holes 4 and 5 suggest that it is still part of the diorite/monzonite suite.

LRC-5

Logged as granodiorite from surface to 202 meters. Strongly weathered near surface, contains limonites and copper oxides, sericite, traces of magnetite, pyrite and chalcopyrite. Rock becomes fresher after 8 meters. Sericite alteration dominant to 42 meters, pale red alteration seen in feldspars to 76 meters (hematitic alteration of sodic plagioclase or potash metasomatism?) Chlorite is present throughout but not strong. Sulphide content is up to 5% at

28 meters--70% pyrite, 30% chalcopyrite. First signs of black mineral (chalcocite?) Sulphide content decreasing after 40 meters. Chlorite alteration increasing between 70 meters and 94 meters, becoming strong between 94 meters and 100 meters. Traces of chalcopyrite and chalcocite to 120 meters as well as red alteration noted previously. Chlorite alteration remains moderate, up 50% of rock has the pale red alteration between 168 meters and 176 meters. Cracked and zoned feldspars seen at 186-188 meters. An olive gray "monzonite" was encountered after 202 meters. Chlorite phenocrysts common (replacing biotite?) Very uniform rock, unmineralized. This sounds like an andesite dyke again.

LRC-6

Quartz porphyry/aplite unit encountered between surface and 68 meters. Abundant magnetite and quartz veinlets throughout, traces of biotite. Oxidized to about 66 meters. Rare traces of pyrite and chalcocite are encountered after 20 meters depth. Granodiorite/quartz monzonite after 68 meters. Chloritized biotite and hornblende?, feldspars show weak to moderate alteration, traces of sericite. Traces magnetite, chalcopyrite, chalcocite and 1% - 3% disseminated pyrite throughout; essentially a weakly mineralized hole.

LRC-7 (Abandoned)

LRC-8

Described as weathered andesite from 0 to 42 meters, but sounds like the aplite/quartz porphyry unit from descriptions: extensive hematite alteration, quartz, biotite, traces magnetite. Possibly an andesite dyke, or dykes, are intermixed with the aplite/quartz porphyry (saussuritized feldspars, sericitized muscovite.) The granodiorite starts at 42 meters and becomes fresher after 48 meters, possibly the weathering boundary. Abundant chlorite, 1-3% disseminated pyrite, traces of magnetite, copper oxides and chalcocite in upper portions of zone. Increase in chalcocite at 68 meters, up to 1%, persists for several meters. Gradational increase in magnetite content (1-3%) after 82 meters, sounds like holes 18, 19 & 20, changing to a more mafic unit classified as "diorite."

LRC-9 (Abandoned)

LRC-9A

Quartz porphyry/aplite phase logged to 42 meters. Zones of pervasive hematite, but limonites are more common. Traces magnetite, chalcocite and pyrite, locally. Granodiorite after 46 meters, increased alteration (clay, sericite), limonite more abundant than hematite. Increased chalcocite after 70 meters, traces copper oxides. Rock becomes fresher after 74 meters (oxidation boundary), chlorite, increased chalcocite, pyrite and chalcopyrite, up to 3%. Trace to 3% chalcocite noted to end of hole (98 meters.)

LRC-10

Aplite/quartz porphyry from surface to 62 meters. Much like in other holes: hematite, quartz, traces magnetite, abundant specular hematite. Poor return in upper portion of this hole, badly broken ground (note drill problems with twin LDD-17.) Traces of chalcocite noted locally. Disseminated stockworks of pyrite and chalcocite seen in upper portion of granodiorite/quartz monzonite unit. Trace to 1% chalcocite and pyrite for several meters.

LRC-11

Encountered granodiorite from 0 to 14 meters, then the quartz porphyry to 34 meters. Traces pyrite, magnetite, quartz, abundant hematite locally, much as before.   Granodiorite after 34 meters with a narrow aplite dyke from 46 to 52 meters. Increase in limonites, pyrite, chalcocite. Strong sericite alteration from 52 to 58 meters (fault zone along which dyke intruded?) Abundant chalcocite to end of hole (92 meters); rods stuck and had to be abandoned. Traces of copper oxides from 80 meters to end of hole.

LRC-12

Granodiorite from surface to 90 meters. Dominantly limonite alteration rather than hematite. Traces pyrite, magnetite, specularite and chalcocite throughout; minor copper oxides from 10 meters to 24 meters. Chalcocite increasing after 42 meters, increased pyrite and chalcopyrite as well, 1% and 0.5%, respectively. Chalcocite content decreases after 94 meters, mafic content increases after this point, as does chlorite.

LDD-13 (Twinned Diamond Drillhole of LRC-9A)

Open-holed with RC to 70 meters. Much the same granodiorite as seen in chips. At least three sets of crosscutting quartz veins visible. Early set of dominantly sulphide rich fractures (pyrite greater than chalcopyrite). Chalcocite increases after 72 meters, estimates from trace to 2.5% chalcocite. Chalcocite clearly seen rimming/replacing chalcopyrite in quartz veinlets and as coatings on pyrite.

LDD-14 (Twinned Diamond Drillhole of LRC-11)

Open-holed with RC to 67 meters. Similar to granodiorite in LDD-13 but contains much more intense quartz veining and sulphides (dominantly pyrite.) Moderate to weak potash feldspar and moderate sericite alteration seen to end of hole. 1-1.5% pyrite and trace to 2.5% chalcocite estimated throughout.

LRC-15

Granodiorite throughout hole. Weathered from surface to about 58 meters. Variable amounts of limonites and hematite throughout weathered (leached) zone, traces of magnetite. Chalcocite and pyrite content increases rapidly below weathered horizon--estimated up to 1% chalcocite, but this was underestimated. Chalcocite decreases after 76 meters, chalcopyrite and pyrite increase (hypogene zone.) Up to 2% disseminated pyrite and 0.5% chalcopyrite.

LRC-16

Collared in aplite/quartz porphyry and penetrated dacite dyke at 32 meters. Abundant hematite, quartz and traces of magnetite. Minor copper oxide seen between 12 meters and 16 meters. No sulphides or quartz in dacite dyke, but lots of manganese minerals (pyrolusite, neotocite, etc.) Copper oxides common throughout but concentrated in two zones: between 38 meters and 46 meters, and between 84 meters and 90 meters, possibly concentrated along faults. Fine biotite phenocrysts throughout dacite--generally fresh in appearance.

LDD-17 (Twin of LRC-10, Abandoned)

Open-holed to 49 meters, diamond drilled to 56.10 meters. Did not penetrate the granodiorite; core is just the quartz porphyry/aplite unit. Lots of quartz veining and hematite but no copper minerals or pyrite. Hole was abandoned due to driller welding bit to bedrock. Badly fractured ground and lost water return twice.

LRC-18

Quartz porphyry from surface to 42 meters. Limonites consist about 20% of rock, includes some hematite. Traces magnetite and quartz veins, some alteration of feldspars (saussaurite), some sericite and chlorite alteration of feldspars and biotite, respectively. Granodiorite to about 72 meters, becomes darker and magnetite content increases after that--best classified as diorite. Traces to 2% pyrite and traces of chalcopyrite in lower part of hole; only local traces of chalcocite. Looks like pyrite halo of system.

LRC-19

Quartz porphyry to 30 meters. Much the same as elsewhere: hematite, magnetite, quartz. Granodiorite/diorite below 30-32 meters. Biotite, quartz, chlorite and traces of chalcocite and pyrite. Increased chalcocite and traces of copper oxides between 42 meters and 58 meters. Very strong magnetite and chlorite, plus pyrite and fresh biotite. Looks like the same diorite/granodiorite unit seen in holes LRC-8 & LRC-18. Traces of potash feldspar between 90 meters and end of hole (96 meters.)

LRC-20

Granodiorite from collar to end of hole; disseminated biotite throughout, moderate magnetite to about 38 meters, then stronger. Leached zone ends at about 28 meters. Traces of copper oxides, chalcopyrite and chalcocite between 36 meters and 54 meters. Quartz porphyry dyke between 48 and 52 meters, granodiorite/diorite below that. Much the same as above but increase magnetite, traces of copper oxides and black mineral grains, possibly chalcocite. Mafic content increases with depth (mostly biotite). Looks like the diorite/granodiorite phase again.

LRC-21

Quartz porphyry from surface to 58 meters. Trace to weak magnetite, abundant quartz eyes, limonites more common than hematite. Vein quartz is common, traces of copper oxides from 44 meters to 64 meters; chalcocite increases from 60 meters. Granodiorite after 58 meters to end of hole. Oxide/sulphide interface at 78 meters, chalcocite content increases here to about 92 meters. Pyrite and chalcopyrite increase with depth in hypogene zone.

LRC-22

Quartz porphyry from 0 to 88 meters. Much the same as elsewhere. Lots of gouge mixed with copper oxides between 28 meters and 42 meters; copper oxides continue to 62 meters. Transition zone from oxide to sulphide phase below 52 meters, chalcocite present and becoming stronger after 86 meters. Changes to primary sulphide zone at contact with overlying aplite/quartz porphyry. Chalcocite content is higher in underlying granodiorite as is pyrite. Moderate to strong sericite alteration locally. Hypogene zone encountered below 110 meters, chalcocite levels drop off and chalcopyrite and pyrite are dominant sulphides. Minor gypsum also visible.

LRC-23

Granodiorite throughout hole. Weak magnetite, traces chalcocite and copper oxides through much of hole. Oxide/sulphide interface at 32 meters. Consistent alteration and lithology throughout. Weakly mineralized with no clear supergene as seen in other holes.

LRC-24 (RC to 46 meters, Core From 46 to 89.7 meters)

Granodiorite/diorite throughout hole. Traces of magnetite, copper oxides and chalcocite in upper part of hole; limonites are stronger than hematite. Increase in chalcocite at 44 meters.   At 46 meters occur 1-2 mm wide, sub-parallel and conjugate fractures trending 30 deg from core axis containing chlorite, quartz and pyrite. Five mm wide quartz veins, containing pyrite and chalcocite crosscut these early veinlets. Lots of zoned plagioclase throughout, >2/3 of total feldspar, so best classified as a granodiorite. Quartz stockwork zones with iron carbonates occur locally, possibly in-filling fault zones. Some secondary (fresh) biotite but chloritized biotites are common. Potash feldspar metasomatism seen locally; seems as if it "overprints" the chlorite

which may represent an earlier phase of propylitic alteration. Essentially, veining and mineralization looks similar to core in hole LDD-13 but not quite as strong.

Mineralization & Interpretation

The target zone drill-tested, so far, lies within an area roughly 500 meters east-west by 500 meters north-south. Drill hole LRC-6 appears to lie west of the area of interest and holes LRC-1 and LRC-3 to the south (see figure 4.) Significant intercepts of supergene copper mineralization were encountered holes LRC-4, 5, 8, 9A/13, 10, 11/14, 15, 19, 21 and 24. The mineralization consists dominantly as fine sooty chalcocite either replacing, or coexisting with chalcopyrite or as thin coatings on pyrite.

The geometry of the Lara porphyry deposit and the fractures that control the mineralization could be considered to be more or less isotropic. Porphyries tend to have a domal, or onion-skinned geometry with mineral and alteration envelopes changing from the nucleus to the outer shells on a very large scale. Post-mineral faulting has offset these mineralized blocks somewhat.

Drill sample intervals were all spaced at 2 meters, and all holes were drilled vertically except for one; the inclined hole was drilled to optimize the terrain and available drill platforms at the time.

Petrographic work performed on two samples collected from hole LDD-13, at 80.5 meters and 86.1 meters, indicate that the host rock is best classified as a granodiorite. Plagioclase has been moderately to intensely altered to sericite and clay minerals (argillic alteration), and biotite has been locally chloritized. Quartz veinlets form intersecting stockworks and pyrite occurs in at least one vein set. Very fine chalcocite occurs mostly as discrete disseminations in 10 micron to 400 micron size particles spatially-related to pyrite, but generally separate from it. The chalcocite replaces fine chalcopyrite, but sometimes is seen rimming it, or occurring as coatings on pyrite.

Three cross-sections are presented in Figures 5 to 7, following; each section is a projection of data 100 meters behind and 100 meters in front of the section line. What is evident from each section is how the supergene zone roughly parallels the topographic profile. On average, the upper
contact of the high grade zone starts somewhere between 60 meters and 80 meters depth, and generally at the interface between the oxidized and unoxidized rock. The younger quartz eye porphyry/aplite unit forms dykes and irregular stock-like and sill-like bodies near the center of the porphyry system and is in direct contact with the supergene zone in holes LRC-10 and LRC-22. This may not have any significance because the quartz porphyry contact is located higher than the supergene zone in all other holes in which it occurs.

The greater than 0.50% copper cut-off (red histograms) reflects a zone of higher grade mineralizaton ranging from 14 meters to 28 meters in thickness and centered roughly about

holes LRC-11/LDD-14. Section 8411200 North (figure 5) shows hole LRC-15 sitting near the topographic summit. Good values exist in hole LRC-12 to the west but start to dwindle in LRC-23, further west and downhill. Three narrow intervals in hole LRC-23 appear to be the projection of the high grade zone and also seem to correlate with the two narrow higher grade zones in the upper parts of holes LRC-4 and LRC-5. The latter two holes lie off-section to the south of LRC-12 and LRC-15. Similarly, to the east, the supergene zone in hole LRC-24 is weaker and narrower.

Figure 7 demonstrates the draping nature of the supergene zone at a consistent level below the surface. The lower portion of LRC-5, penetrating the section from the southeast, shows low grade copper mineralization (0.10% to 0.50%) in the hypogene zone from 80 meters to 150 meters below surface. The last 50 meters (+/-) is within a barren andesite dyke.
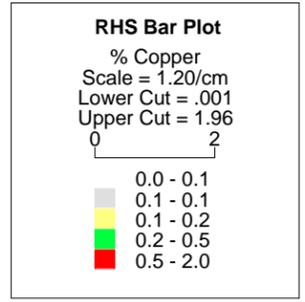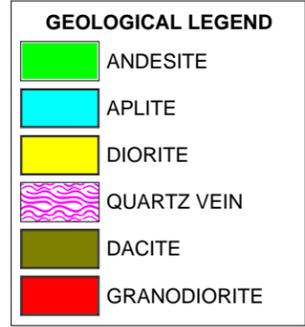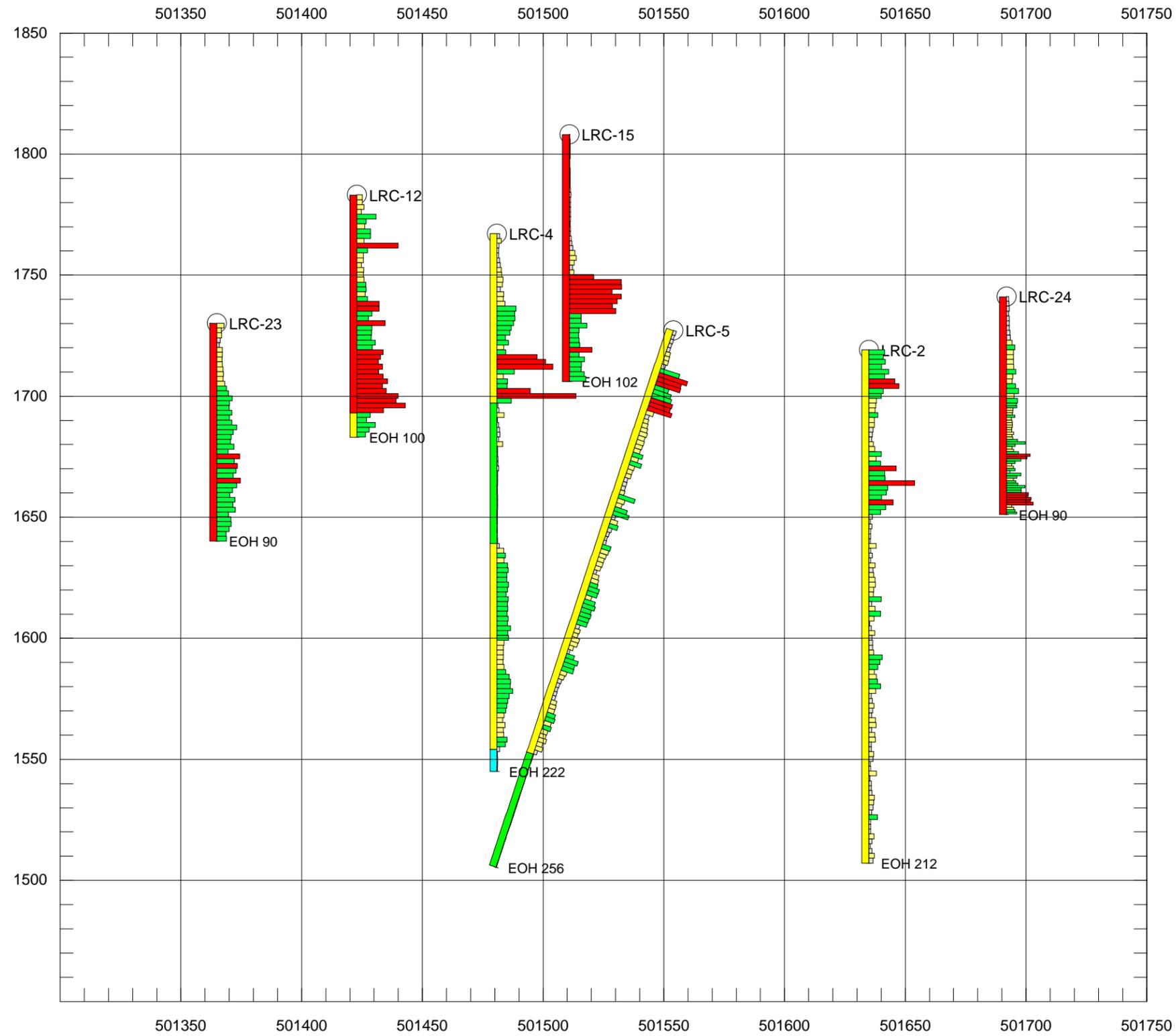
Sampling Method & Approach

Eighty rock chip samples were collected by Villafuerte and the author between 1994 and 1997 from within the area of the claims as shown on Map 1 (in pocket). The sampling procedure undertaken by Villafuerte is unknown. The author cleared outcrop, or subcrop, of colluvial detritus for a "fresh" sampling surface. A geologist's hammer was used to collect the samples; the
rock was sufficiently altered to not require the use of a chisel. Individual samples ranged from 2 to 5 kg, approximately.
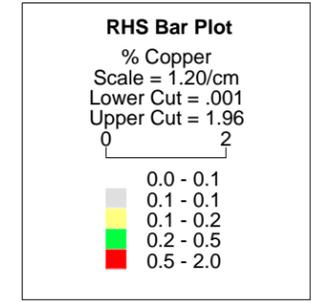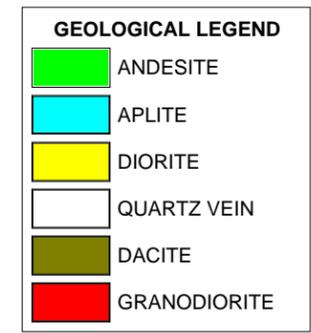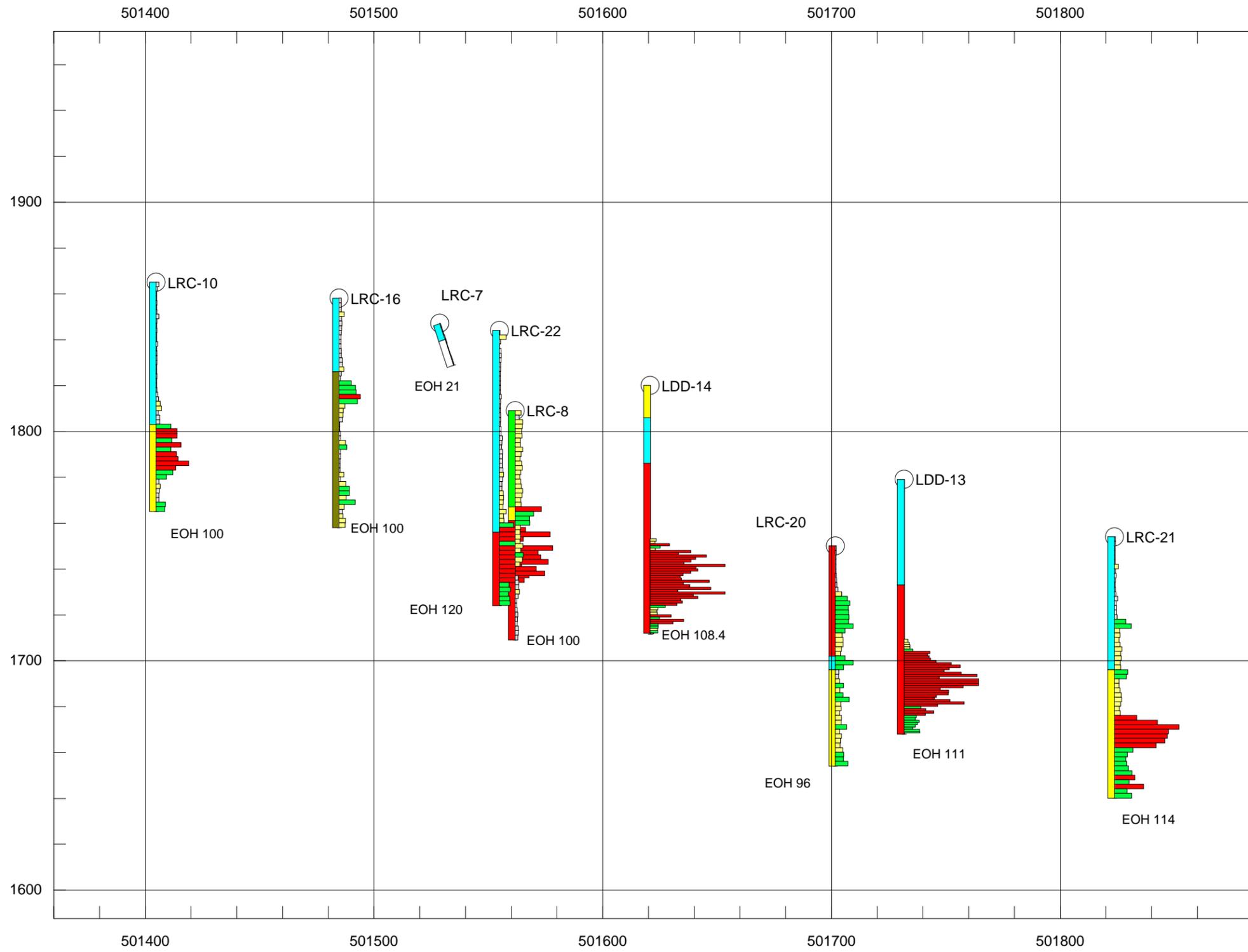
The area covered by both Villafuerte and the author is roughly 3 km east-west by 2 km north-south, or 6 square km. This works out to roughly 13 samples per square km.

All the drill hole collars were surveyed using an Ushicata Tracon S-25 transiting theodolite and chain; the theodolite has precision of +/- 1 minute. Station 0, located at drill hole LRC-6, near the western end of the crest of the ridge underlying the target area, was used as a reference point for the transit survey. A relative UTM coordinate of 501,237 meters east and 8,411,624 meters north was determined using a Trimble Scout (model 17319) GPS instrument, having a precision ranging from 3 to 300 meters, depending on the number of satellites detected and number of readings taken. A relative elevation of 1860 meters was also determined using this same instrument. A starting azimuth was determined using a compass built into the theodolite; The theodolite survey ties in all the drill holes, roads and platforms in the target area but does not triangulate, or close, with the origin or other points along the survey. As such, this is an "open" rather than "closed" traverse, so the survey data could not be balanced.

 The collected data was compiled in digital format by the author and processed using the Rockware survey utility. This program reduces azimuth, inclination and chain data to coordinate X, Y & Z values relative to a known point (LRC-6.) The data points generated were imported into an older CADD geology drawing of the property. Only one bad data point was noticed, causing drill holes LRC-2 and LRC-5 to be too close together. This turned out to be

GEOLOGICAL LEGEND

Color	Rock Type
(green)	ANDESITE
(cyan)	APLITE
(yellow)	DIORITE
(pink/hatched)	QUARTZ VEIN
(olive)	DACITE
(red)	GRANODIORITE

RHS Bar Plot

% Copper
Scale = 1.20/cm
Lower Cut = .001
Upper Cut = 1.96

0   2

Color	Value
(grey)	0.0 - 0.1
(light)	0.1 - 0.1
(yellow)	0.1 - 0.2
(green)	0.2 - 0.5
(red)	0.5 - 2.0

LRC-15

LRC-12

LRC-4

LRC-23

EOH 102

LRC-5

LRC-24

EOH 100

LRC-2

EOH 90

EOH 90

EOH 222

EOH 256

EOH 212

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0   40   80   120

Scale 1:2000

GEO: JN	SCALE 1:2000	PAGE: 28
DRAWN: JN	'DATE: 09-02-2004	PLAN: Fig. 5

GEOLOGICAL LEGEND

- ANDESITE
- APLITE
- DIORITE
- QUARTZ VEIN
- DACITE
- GRANODIORITE

RHS Bar Plot

% Copper
Scale = 1.20/cm
Lower Cut = .001
Upper Cut = 1.96

0   2

- 0.0 - 0.1
- 0.1 - 0.1
- 0.1 - 0.2
- 0.2 - 0.5
- 0.5 - 2.0

LRC-10
LRC-16
LRC-7
EOH 21
LRC-22
LRC-8
LDD-14
EOH 100
EOH 100
EOH 120
EOH 100
LRC-20
LDD-13
EOH 108.4
LRC-21
EOH 96
EOH 111
EOH 114

0   40   80   120
Scale 1:2000

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WESTERN PERU
SECTION 8411400 N0RTH

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| DRAWN: JN | 'DATE: 09-02-2004 | PLAN: Fig. 6 |
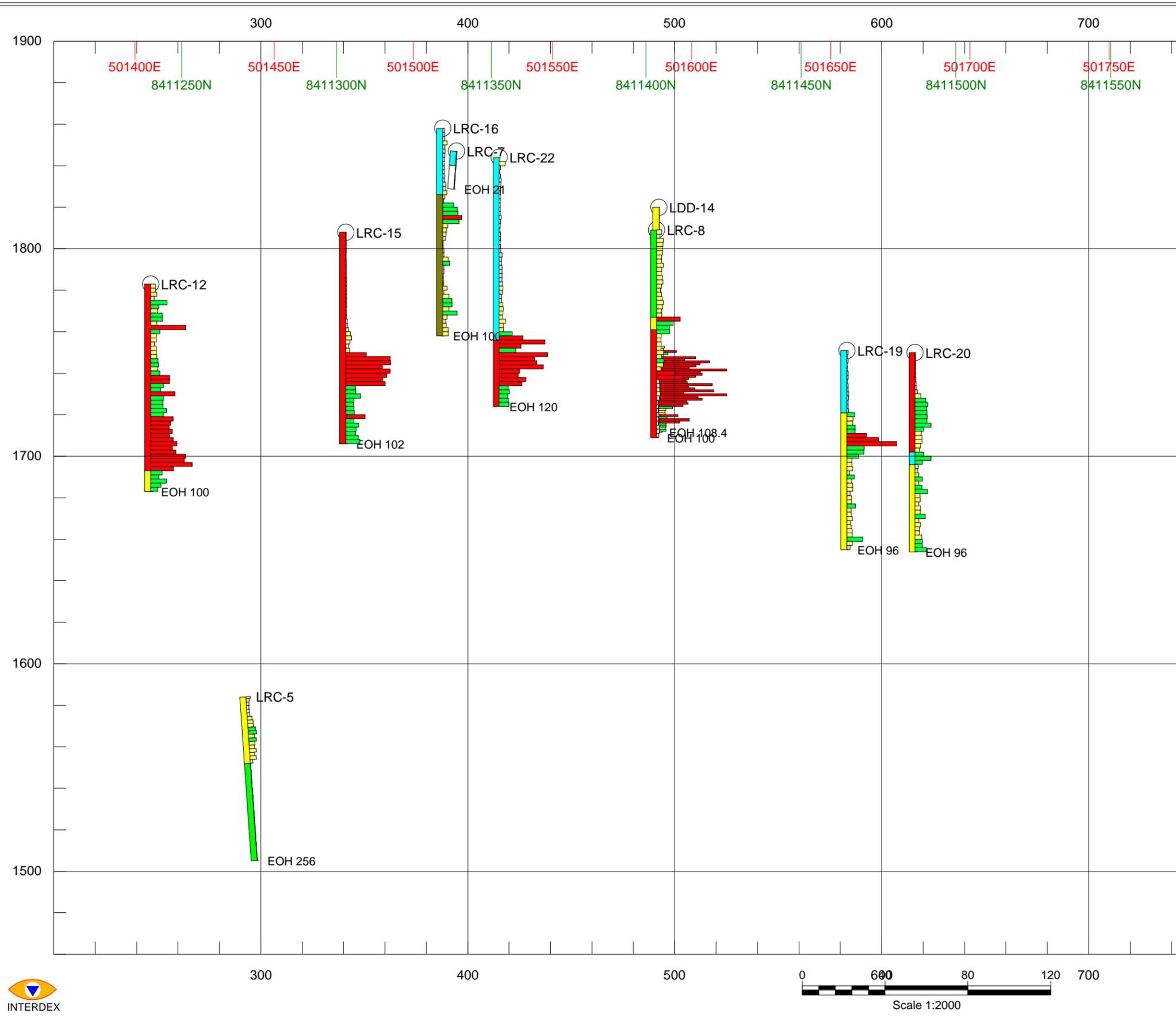
GEOLOGICAL LEGEND

- ANDESITE
- APLITE
- DIORITE
- QUARTZ VEIN
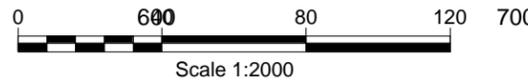- DACITE
- GRANODIORITE

RHS Bar Plot

% Copper
Scale = 1.20/cm
Lower Cut = .001
Upper Cut = 1.96

0 ————— 2

- 0.0 - 0.1
- 0.1 - 0.1
- 0.1 - 0.2
- 0.2 - 0.5
- 0.5 - 2.0

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WESTERN PERU
SECTION SW-NE

| GEO: JN | SCALE 1:2000 | PAGE: 30 |
| DRAWN: JN | 'DATE: 09-02-2004 | PLAN: Fig. 7 |

Scale 1:2000

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just a clerical labelling error and not an error in the survey itself. Without the benefit of a closed traverse, an estimate of the survey accuracy is strictly speculation; a location accuracy within a few meters would be expected, and the error would be greater further away from the origin point (LRC-6.)

A 5 1/4" diameter drill head was used in all the reverse circulation drill programs. The diamond drilling was performed with the same reverse circulation drill rig by switching the drill from a pneumatic to a hydraulic head, a procedure that took about 3 hours. The entire core section in all three holes was drilled using HQ diameter bits and rods. The drill core was logged on site and shipped to Lima to be sawn in half for sample preparation and analyses.

Reverse circulation (RC) drilling has some deficiencies not found in core drilling. Rock chips and fines can pass into fractures and open spaces in the rock being drilled; a certain amount of sample also blows past the drill stem onto the ground. There is also a certain lag time at depth for sample material to reach the surface. This could affect sample spacing somewhat when compared to drill core at the same depth.

A comparison of core vs. chip samples from two twinned holes is discussed in a later section. Briefly, the analyses suggest that core drilling recovers more fine chalcocite than the RC method, for the reasons mentioned previously.

Lithologies had no bearing on the sample interval selection (2 m), as mentioned earlier.

Sample Preparation, Analyses and Security

Samples were for the most part collected dry and split using a Jones sample splitter. Two samples, roughly 8 kg each, were taken--one for laboratory analyses, another as a duplicate for storage. Drill holes LRC-1 and LRC-2 encountered water at 27 meters and 177 meters, respectively. Hole LRC-9 was drilled wet below 70 meters, LRC-16 below 40 meters, LRC-20 below 80 meters and LRC-22 below 76 meters. The wet samples were passed through the Jones splitter as well, and each sample pass was thoroughly washed out before the next sample was split. The wet samples were air dried before being packed and shipped to the laboratory.

All samples were collected by junior field employees of Minas Dixon; a Minas Dixon geologist or the author were on site to supervise the drilling and sampling as well as to collect small specimens of chips for logging.

A duplicate check sample was collected and submitted from every tenth and fourteenth sample, alternately, as one form of quality control. The results of these duplicate samples matched adequately with the original sample.

All reverse circulation chip samples and the split drill core from all three drilling programs were analyzed for total copper at Plenge Laboratories, Lima, Peru. For total copper, the samples were

digested in 1.5:1 ratio perchloric-nitric acid solvent for 12 hours at 80 deg. C. The cooled solute was reduced to 10 ml with 2:8 ratio hydrochloric acid-water solution and analyzed with a Perkins- Elmer 5100 atomic absorption instrument. Two samples are repeated every 24 samples and one internal standard and one blank sample is analyzed every 24 samples. The check samples compared favourably throughout. The standard has a value of 42 ppm with a deviation of +/- 2 ppm; the lower and upper detection limits are <2 ppm Cu and 10,000 ppm Cu (1:10 dilution), respectively.

In the first drilling program the Company had pulps from roughly every tenth sample sent to International Plasma Laboratories (IPL), Vancouver, B.C., for check analyses. A 0.5 g sample was digested with aqua regia and analyzed for copper and multi-elements by ICP (inductively coupled plasma spectrophotometry) technique. A sample batch consists of 38 or fewer samples. An in-house standard and an acid blank are placed before each sample batch. A known standard with characteristics best matching the samples is chosen and placed after every fifteenth sample. After every 38th. sample (not including standards), two samples, chosen at random, are re-weighed and analyzed. At the end of a batch, the standard and blank used at the beginning are rerun. The readings for these knowns are compared with the pre-rack knowns to detect calibration drift. This procedure is used for both atomic absorption and inductively coupled plasma spectrophotometry methods.

In addition, the samples from the first program were analyzed for molybdenum, gold and soluble copper by Plenge Laboratories. For molybdenum, a 0.5 g sample was digested in a nitric-perchloric acid solution to which 0.5 ml of aluminum chloride and 20% hydrochloric acid was added to make 10 ml volume. The solution was analyzed with a Perkins Elmer 5100 atomic absorption instrument. Two samples are repeated every 24 samples and one internal standard and one blank sample is analyzed every 24 samples. The instrument has a 2 ppm detection limit with an upper detection limit of 1,000 ppm (1:10 dilution.) The internal standard has a nominal 2 ppm value with a deviation of +/- 1 ppm.

Gold was analyzed using fire assay and atomic absorption finish. A 30 g sample was mixed with Asarco "Pueblo Brand" litharge and other fluxes, as appropriate. The bullion is leached with a nitric acid-water solution to dissolve excess silver; the remaining bullion bead is disolved with aqua regia and analyzed with the above-mentioned atomic absorption instrument. The samples were checked with duplicates and an internal standard as described previously. The atomic absorption instrument has lower and upper detection limits of 5 ppb Au and 10 ppm Au, respectively. The internal standard is 92 ppb Au +/- 3 ppb Au. The gold values were very low and are not documented in this report; the average values are in the 0.00X ppm to 0.0X ppm Au range.

Soluble copper (copper carbonates) was also analyzed by Plenge Laboratories.   A 0.500 g sample is digested in a 9:1 ratio sulfuric acid-water solvent. The sample is shaken in a test tube for 120 minutes, centrifuged for 10 minutes, then analyzed by atomic absorption, as described

previously. The lower and upper detection limits, respectively, are <2 ppm Cu and 10,000 ppm Cu (1:10 dilution.)

During the second drilling program, the pulps from all samples that ran greater than 2000 ppm Cu were sent to IPL in Vancouver for check analysis. The samples in Vancouver were digested in multi-acids and assayed for total copper using atomic absorption technique. A 0.50 g sample is digested in aqua regia at 95 deg. C. for 90 minutes, cooled and made up to a fixed volume with de-mineralized water. Each element is determined by comparison with a set of known standards. The AA machine is first calibrated with three known standards and a blank; the test samples are then run in batches with blanks and standards interspersed as described earlier.

In addition, the samples were analyzed at IPL for soluble copper using sulphuric acid digestion and atomic absorption technique. A 0.50 to 2.00 g sample of -200 mesh material is dissolved in 100 ml of 10% sulphuric acid, with a pinch of paper pulp. After 2 hours of stirring, the sample was filtered and washed 4 times with distilled water. The sample was taken up to a fixed volume, agitated, and analyzed by an atomic absorption instrument. An internal standard or blank and a random repeat are digested and analyzed with every 38 client samples.

The check analyses done at IPL compare favorably with the original results obtained at Plenge Laboratories; the total copper digestion and assay technique performed at IPL did not seem to significantly enhance the copper values.

Again, during the third program all samples that ran greater than 2000 ppm Cu were sent to IPL in Vancouver for check analysis. Instead of using the original pulp, a second split was taken of the minus 10 mesh material. IPL Laboratories performed geochemical and assay level analyses on this second split.

One-half of the sawn drill core was crushed to minus 1/2" at Plenge Laboratories in Lima. This crushed material was split equally, and one-half was saved for an upcoming bottle roll and column leach study to be conducted by Plenge Laboratories. The other half of the -1/2" material was crushed to -10 mesh, and separate samples were taken from this material for geochemical and assay level copper analysis in Vancouver and two geochem analyses in Lima. As a result, the reverse circulation samples from the third program have three separate analyses and the drill core samples have four separate analyses performed on them.

The Company did not include any "blank" or certified "standard" samples in any of the drilling programs.

IPL is a member of Canadian Association of Environmental Analytical Laboratories (ACLAE), a member of Mineral Analysis Laboratories Council of Canada, a participant of Proficiency Testing Program for Mineral Analyses Laboratories (PTP-MAL) and is ISO9002 certified by KPMG.

The professional associations that Plenge Laboratories, Lima, Peru is a member of is unknown to the author.

In my opinion, the quality control and checks that were implemented in the three drilling programs were adequate and served their purpose. No analytical anomalies or significant abberations were detected from within the mineralized zones, nor were there any irregular values reported from zones where mineralization was not noted. In future, I would recommend that the Company adopt a policy of inserting a blank and certified standard sample at a regular yet random basis within their sample suites prior to shipment to the lab.

Data Verification

A discussion of quality control methods was documented in the preceding section.

The author was employed as a consultant by the Company during all drilling programs. I reviewed and compiled all results as they became available from either Plenge Laboratories, Lima
or IPL Laboratories, Vancouver. I have visited the facilities of both laboratories.

Field logging and sampling was either observed by, supervised by, or personally conducted by the author in all three drilling programs. The entire third program was directly supervised by the author.

Verification of data was performed by the checks outlined above. No problems were encountered in the reporting except for minor clerical errors that were later corrected in logs, etc. Nothing out-of-the-ordinary was noted in the analytical reports, and they all appeared to be authentic, whether faxed originals or subsequent hard copies or digital files.

A discussion of comparisons of some composite analyses between the two laboratories and between reverse circulation and diamond drill core samples follows.

Comparison of Analyses Between Laboratories

Table 3, below, shows the composited averages of the most significant intervals for the analyses obtained from each laboratory, where applicable; the individual samples are listed in Appendix I. In summary, the values compare very favourably between laboratories with IPL's values being just slightly higher. The assay technique generally did not enhance the geochemical values significantly.

Comparison of Assays Between Drill Core and Drill Cuttings

Diamond drill holes LDD-13 and LDD-14 are twins or reverse circulation drill holes LRC-9A and LRC-11, respectively. The purpose of the diamond drilling was to see if core samples

would enhance the copper grades because fine sulphides are often lost with reverse circulation or percussion drilling techniques.

Aside from the two different drilling/sampling methods, the reverse circulation samples were collected at 2 meter intervals while the core was sampled at 1 meter intervals.   The sample numbers shown below belong to the reverse circulation holes, but the sample numbers for the core are not shown because the copper assays for the same intervals are averages of two adjacent 1 meter samples.

Table 3. Comparison of Analyses Between Plenge Laboratories,
**Peru and IPL Laboratories Vancouver, Canada**

Hole	Type	From (m)	To (m)	Width (m)	Plenge Labs original	Plenge Labs check	IPLLabs original	IPLLabs check
LRC-9A	RC	74	98	24	11167			10950
LRC-10	RC	62	86	24	5092			5308
LRC-11	RC	70	92	22	6897			7318
LRC-12	RC	52	100	48	5713			6192
LDD-13	DD	74	104	30	10950	11390	11713	11563
LDD-14	DD	69	97	28	10821	11152	11077	11104
LRC-15	RC	58	80	22	9055		8995	9355
LRC-16	RC	36	46	10	4465		4536	4420
LRC-19	RC	30	52	22	4819		4750	5182
LRC-20	RC	22	38	16	3469		3645	3500
LRC-21	RC	78	114	36	7401		7850	8006
LRC-22	RC	84	110	26	8361		8500	8531
LRC-23	RC	26	90	64	3787		4009	4025
LDD-24	DD	73	86	13	4187	4181	4231	4092

 * all values reported in ppm.

The table below shows quite an erratic distribution in copper grades between the core and chip samples. Results from holes LRC-9A and LDD-13 show a variation in copper grade ranging from a 58.88% decrease to a 48.18% increase in the core samples. Holes LRC-11 and LDD-14 show much the same pattern with a variation in copper assays ranging from a decrease of 93.70% to an increase of 77.80%. A 24 metre interval in LDD-13 and a 20 metre interval in LDD-14, diamond drill twin holes of LRC-9A and LRC-11, respectively, significantly upgraded copper
values in the reverse circulation holes by 9% and 72%. The reverse circulation drilling appears to be underestimating copper grades and further diamond drilling is required to verify this
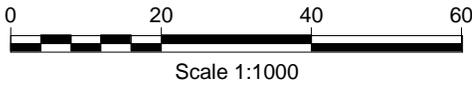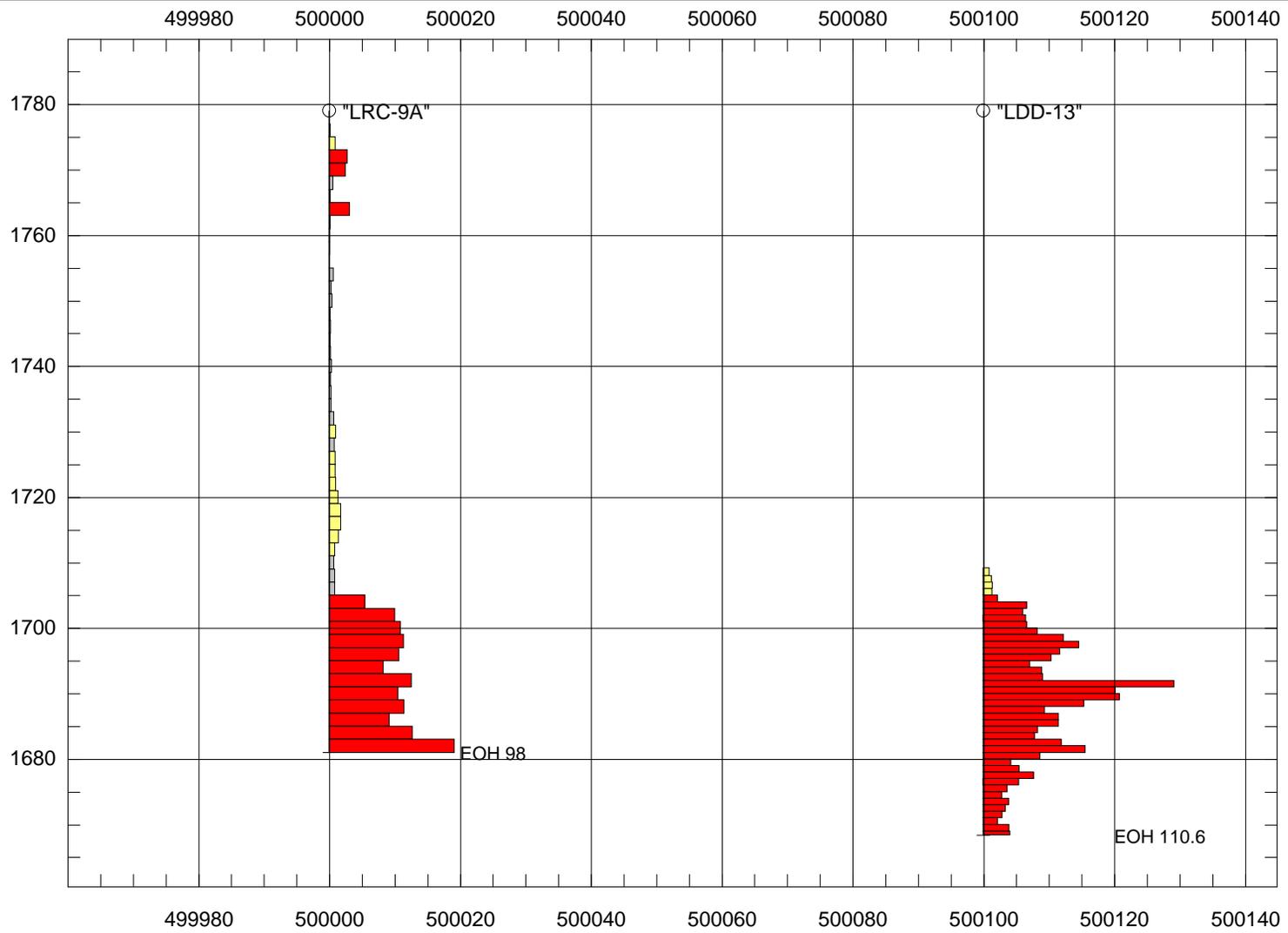
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LARA PORPHYRY COPPER PROJECT
COMPARISON OF ASSAYS BETWEEN
HOLES LRC-9A AND LDD-13

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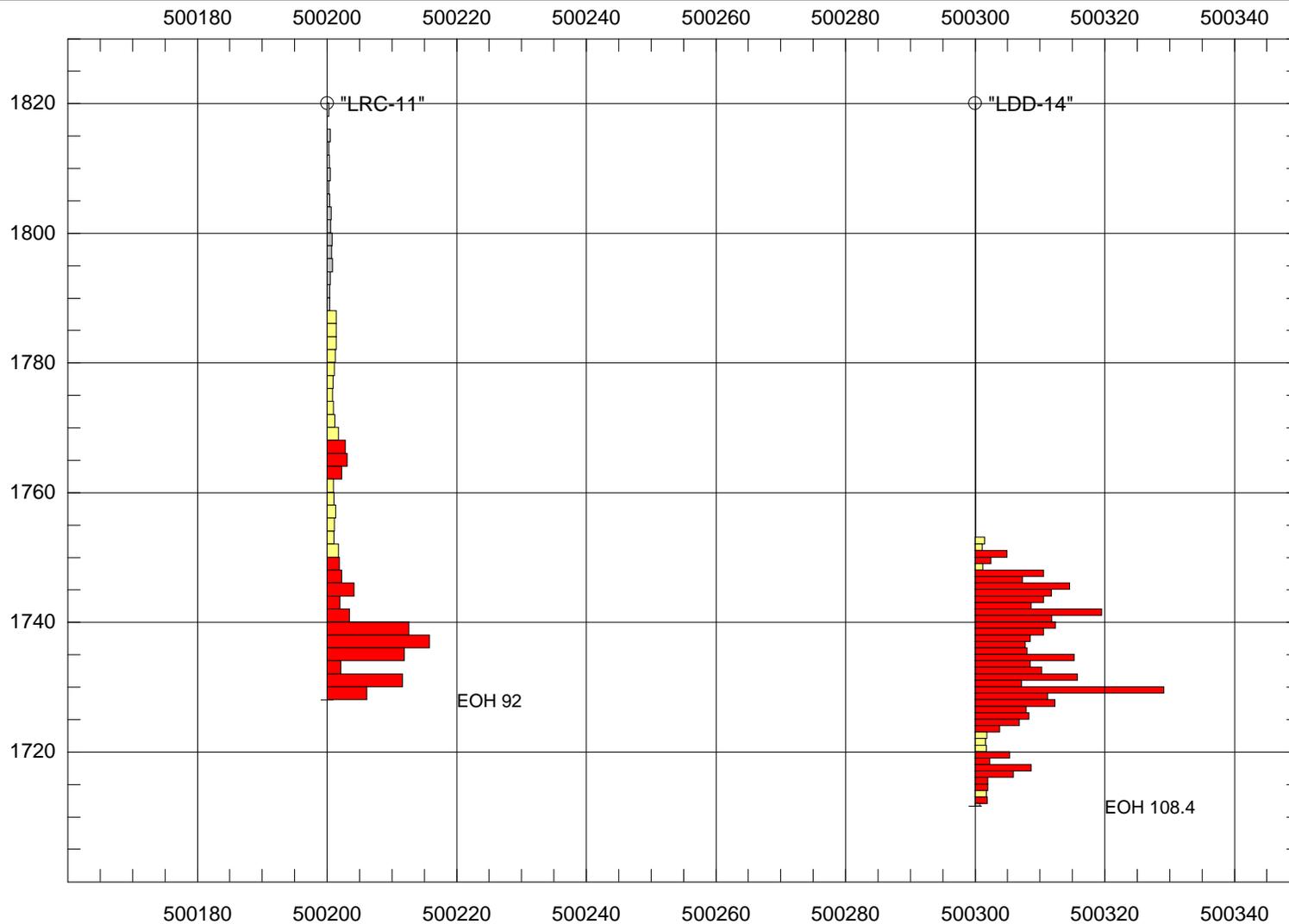
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COMPARISON OF ASSAYS BETWEEN
HOLES LRC-11 AND LDD-14

| GEO: JN | SCALE 1:1000 | PAGE: 37 |
| DRAWN: JN | 'DATE: 09-02-2004 | PLAN: Fig. 9 |

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Scale 1:1000

EOH 92

EOH 108.4

postulation. The exact cause and nature of this loss is not known, but the petrographic work done on the two specimens from hole LDD-13 indicates that chalcocite particulates exist over a range from 10 microns to 400 microns in size. The grade of mineralization has many times been underestimated during logging, and if much of this material is less than say, 250 microns (0.25 mm), then it would not be readily visible. Most of the chalcocite seen in the panned samples occurs as coatings on pyrite grains, and the petrographic report indicates that this is rare compared to the disseminated chalcocite that has either partially or totally replaced chalcopyrite. A percentile distribution of the chalcocite grain sizes has not yet been done on these specimens. Figures 8 and 9 show the relationship between the respective diamond drill and reverse circulation drill holes. The upper contacts of the supergene zone are quite clear and at the same horizon. A few more high grade "spikes" appear in the core samples, and the upper portion of the core in hole LDD-14 shows higher copper values than the corresponding reverse circulation samples.

Table 4. Comparison of Reverse Circulation & Diamond Drill Assays

From (meters)	To (meters)	Hole	Sample	Copper R.C. (ppm)	Hole	Copper DDH (ppm)	% Difference
70	72	LRC-9A	7016	1000	LDD-13	1210	17.36%
72	74	LRC-9A	7017	1000	LDD-13	1520	34.21%
74	76	LRC-9A	7018	5600	LDD-13	4525	-23.76%
76	78	LRC-9A	7019	10200	LDD-13	6420	-58.88%
78	80	LRC-9A	7020	11000	LDD-13	7580	-45.12%
80	82	LRC-9A	7021	11500	LDD-13	13550	15.13%
82	84	LRC-9A	7022	10800	LDD-13	11155	3.18%
84	86	LRC-9A	7023	8400	LDD-13	17050	-2.63%
86	88	LRC-9A	7024	12700	LDD-13	19235	33.97%
88	90	LRC-9A	7025	10700	LDD-13	20650	48.18%
90	92	LRC-9A	7026	11600	LDD-13	12530	7.42%
92	94	LRC-9A	7027	9350	LDD-13	11640	19.67%
94	96	LRC-9A	7028	12850	LDD-13	8220	-56.33%
96	98	LRC-9A	7029	19300	LDD-13	13890	-38.95%
			Averages and Percent Increase	11,167		12,204	9.29%**
66	68	LRC-11	7112	1190	LDD-14	1580	24.68%
68	70	LRC-11	7113	1935	LDD-14	3160	38.77%
70	72	LRC-11	7114	2100	LDD-14	1995	-5.26%
72	74	LRC-11	7115	2400	LDD-14	9070	73.54%
74	76	LRC-11	7116	4300	LDD-14	13320	67.72%
76	78	LRC-11	7117	2170	LDD-14	9775	77.80%
78	80	LRC-11	7118	3600	LDD-14	15830	77.26%
80	82	LRC-11	7119	12800	LDD-14	11610	-10.25%
82	84	LRC-11	7120	16000	LDD-14	8260	-93.70%
84	86	LRC-11	7121	12100	LDD-14	11825	-2.33%
86	88	LRC-11	7122	2300	LDD-14	9545	75.90%
88	90	LRC-11	7123	11800	LDD-14	11600	-1.72%
90	92	LRC-11	7124	6300	LDD-14	26180	75.94%
			Averages and Percent Increase	7,377		12,702	72.18%**

** percent increase of averages between R.C. and core sample analyses, not an average of percent difference between individual samples as shown in column above these values.

Adjacent Properties

There exist no adjacent mineral properties, known to the author, the Company, or documented in the public domain that are comparable in scope or development to the Lara property. As such, no data from any said adjacent property was in anyway incorporated in, or discussed in the body of this document.

Mineral Processing and Metallurgical Testing

In September 1998, a column leach test and a bottle roll test was initiated at Plenge Laboratories, Lima on drill core selected from the supergene zone encountered in drill holes LDD13 and LDD14. Twenty-four contiguous samples from each hole (#'s 9953 to 9976 and 9994 to 10017, respectively) were crushed to 100% - 1/2". A Jones splitter was used to split a representative portion for assay (see results in Appendix I.) The intervals for holes LDD13 and LDD14 averaged 1.30% and 1.25% total copper, respectively.

Taking equal sample weights, the rejects from both sample lots were composited separately. The composites were homogenized and a representative sample was taken and assayed with the following results:

Table 5. Assays from Composite Drill Samples

	LDD13	LDD14
Cu Total	1.28%	1.23%
Cu Soluble in H_2SO_4	0.22%	0.55%
Cu Soluble in NaCN	1.15%	0.98%
Cu Soluble in Acetic Acid	0.13%	0.38%
S Total	2.74%	2.73%
S as Sulphide	1.80%	1.53%
Fe	3.39%	3.08%

A preliminary bottle roll test at 10 mesh was performed on each composite. Results were as following:

Table 6. Bottle Roll Leach Results

Lot	Test No.	*Head Cu%	Residue Cu%	Extraction Cu%	H_2SO_4 kg/tonne	**EMF mv
LDD13	5182-1A	1.35	0.55	59.1	14.5	338
	5182-1B	1.31	0.52	60.4	14.5	338
	Average	1.33	0.535	59.8	14.5	338
LDD14	5183-1A	1.34	0.38	71.6	14.5	348
	5183-1B	1.35	0.37	72.7	13.4	349
	Average	1.345	0.375	72.2	14	348

* calculated head: residue + solution

** Ag/AgCl

The bottle roll leach test indicates copper extractions of 59.8% and 72.2% with sulfuric acid consumption of 13.4 to 14 kg/tonne for lots LDD13 and LDD14, respectively. The high extraction of copper indicates that the ore should be amenable to acid heap leaching.

A column leach test was performed on each sample lot crushed to 1/2", nominal. The following table summarizes the results.

Table 7. Column Leach Test, -1/2" Material

Lot	*Head Cu%	Residue Cu%	Extraction Cu%	**H_2SO_4 kg/tonne	time days	***EMF mv
LDD13	1.39	0.13	90.6	19.58	161	481
LDD14	1.32	0.17	87.1	15.92	154	407

The report by Plenge Laboratories also shows a table listing percent copper extraction vs. particle sizes of 1/2", 1/4" +10 mesh and -10 mesh. It is not documented within that report how the sizes other than the 1/2" material (column leach) were sampled and analyzed. The calculated results show that LDD13 and LDD14 had 90.2% and 86.3% of their copper extracted, respectively.

Observations and conclusions made by Plenge Laboratories include:

- Approximately 90% of the copper minerals are secondary copper (chalcocite, covellite and bornite) as shown by the cyanide leach assay, and less that 8% to 10% is present as chalcopyrite. This is confirmed by the column leach test. The ore should be amenable to bio-heap leaching with expected recoveries in the range of 87% to 91% and sulphuric acid consumptions of 16 to 20 kg/tonne.
- Crushing the mineralized material to 100% -1/4" should result in recoveries in excess of 90% for both samples.
- Sulphuric acid indicates acid generation by the mineralization due to sulphide oxidation and low acid consumption by the gangue material.
- The final pregnant leach solution (PLS) EMF for LDD13 was 481 mv, indicating that almost all iron in the PLS is in the ferric form, and consequently, solphides oxidation was near completion.
- The final EMF for PLS from LDD14 was 407 mv, suggesting that sulphide oxidation was not as complete as LDD13 and that a longer leach time is required.

Mineral Resource Estimates

Figure 10 shows the location of all drill holes and roads in the target area, and Figure 11 is a plan view of the polygonal blocks used by the author in calculating a resource estimate in the

central core of the target area. Drill holes LRC-1 and LRC-3 lie southeast of this area and the drawing, and although LRC-3 contains 26 meters averaging 0.34% copper and 54 meters averaging 0.28% copper, they were not used in this estimate. Hole LRC-6, to the northwest, contains only sub-economic levels of copper and was not used in the estimate either.

Resource estimates were obtained by using the method of polygons, constructed as perpendicular bisectors at the mid-points between adjacent vertical drill holes. Drill hole spacing ranges from
70 meters to 172 meters, but most are under 110 meters apart. The drilling density is sufficient to assume a continuity of mineralization between the holes, even though systematic surface sampling has not been done along roadcuts. The Company has not conducted such a sampling program because the rock is extremely leached and would likely return only geochemically anomalous values, as indicated in the mapping and sampling survey conducted by the author in 1995.The drilling density is believed sufficient to tentatively classify the in-situ mineralization as an *inferred resource.*

Some parameters used in this calculations include:

1. Hole LRC-5 is angled at -60 degrees inclination at 325 degrees azimuth. The midpoint of this hole is deemed to be the "vertical" collar site and its polygonal block was drawn around this point.
2. The perimeter of the outermost blocks is located at a distance not exceeding half the distance between the adjacent outermost holes. This distance varies from 50 meters to about 65 meters.
3. A density of 2.6 is assumed for the mineralized rock. An average density (specific gravity) for solid, unaltered granitic type rocks is 2.667, and for granodiorite the average density is 2.716. A series of density measurements will be required to obtain an appropriate value. A total of 2,042 measurements were made at the Andacolla mine in Chile; values ranged from 2.25 in leached fault gouge to 2.59 in supergene trachyte. The host rocks at Andacolla are largely sediments and volcanics, but it is not stated whether an average density was used in resource/reserve calculations or if the calculations were determined using average values for individual lithologic units (Libby et al, 1998.)
4. The areas of the polygons were determined using CADD.
5. Weighted averages, volumes and tonnages were calculated using a spreadsheet program.
6. Mineralized thicknesses ranged from 1 m to 64 m; the main zone averages about 30 m (by visual inspection, the reader is referred to Tables 8 & 9, following.) No minimum thickness parameters were employed--these are "global" resources.

Two inferred resource estimates are calculated: one using a 0.20% copper cut-off and the other a 0.50% copper cut-off. A 0.2% recoverable copper cut-off grade was used at the Andacolla mine. "Recoverable copper" is defined as that copper that could be determined using sulphuric acid digestions (copper carbonates) and cyanide digestions (chalcocite.) The amount of copper

LRC-6
LRC-18
LRC-19
LRC-10/17
LRC-20
LRC-8
+ 8411400N
502000E
LRC-16
LRC-11/14
LRC-9A/13
LRC-21
LRC-22
LRC-15
LRC-24
LRC-12
LRC-23
LRC-4
LRC-5
LRC-2
501300E
+ 8410900N
LRC-1
LRC-3

0   100   200   300   400 Metres

	LARA EXPLORATION LTD.		
	LARA PROPERTY, PERU		
	DRILL HOLES & ROAD LOCATIONS		
SCALE	DATE	DRAWN BY	FIGURE
1:5,000	FEB. 9, 2004	JN	10

FIGURE10.GCD

LRC=18

LRC=19

LRC=6

LRC=20

LRC=10/17

LRC=8

LRC=9A/13

LRC=11/14

+ 501300E

LRC=16

LRC=21

+ 8411300N

LRC=22

LRC=15

LRC=12

LRC=24

LRC=5

LRC=23

LRC=4

LRC=2

+ 501800E

+ 8411000N

LEGEND

Projected vertical collar
at mid=point of inclined hole

Actual collar of hole LRC=5

0   100   200 Metres

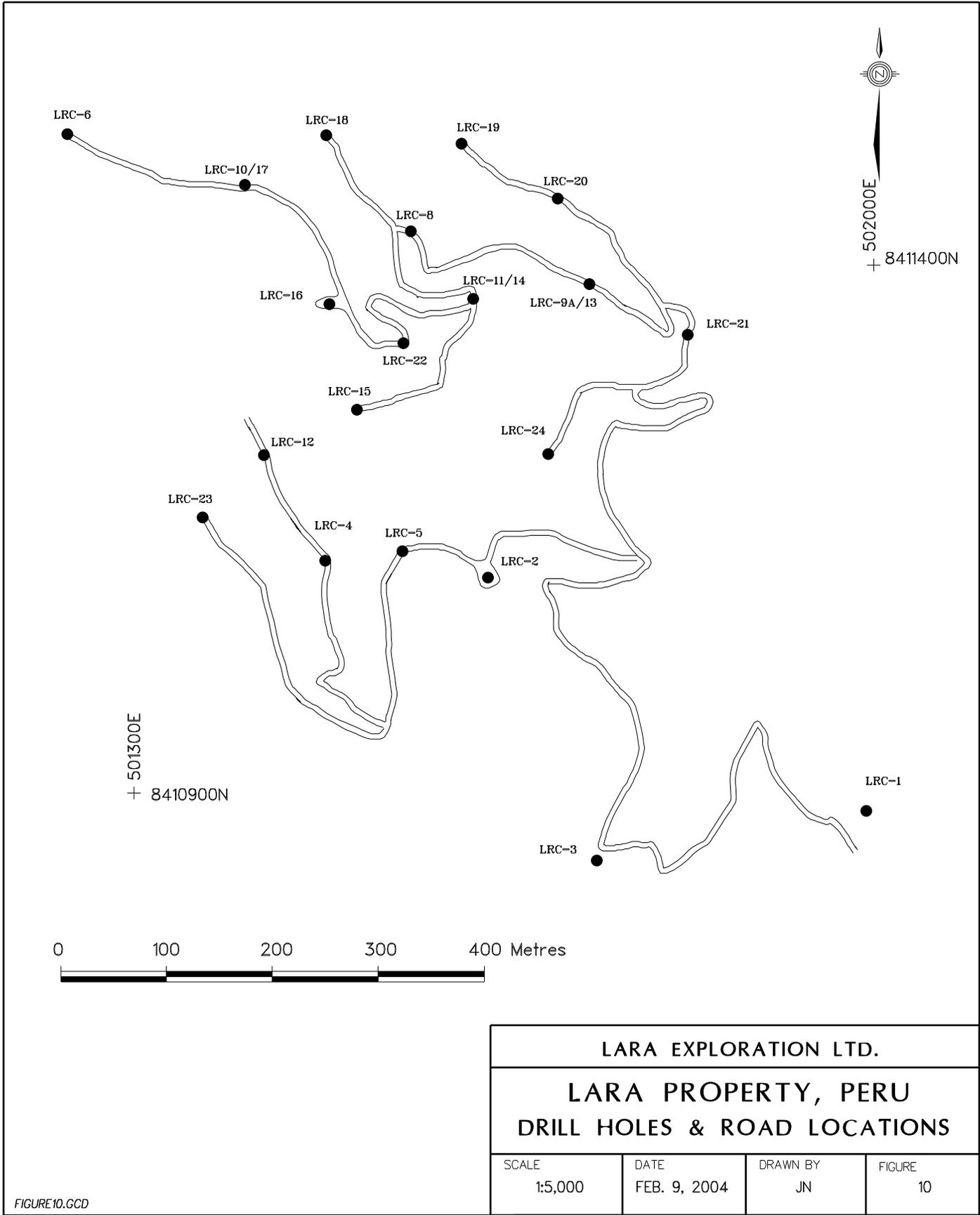| LARA EXPLORATION LTD.			
LARA PROPERTY, PERU			
POLYGONAL RESOURCE BLOCKS			
SCALE 1:4,000	DATE FEB. 9, 2004	DRAWN BY JN	FIGURE 11

FIGURE11.GCD

PGS Pacific Geological Services
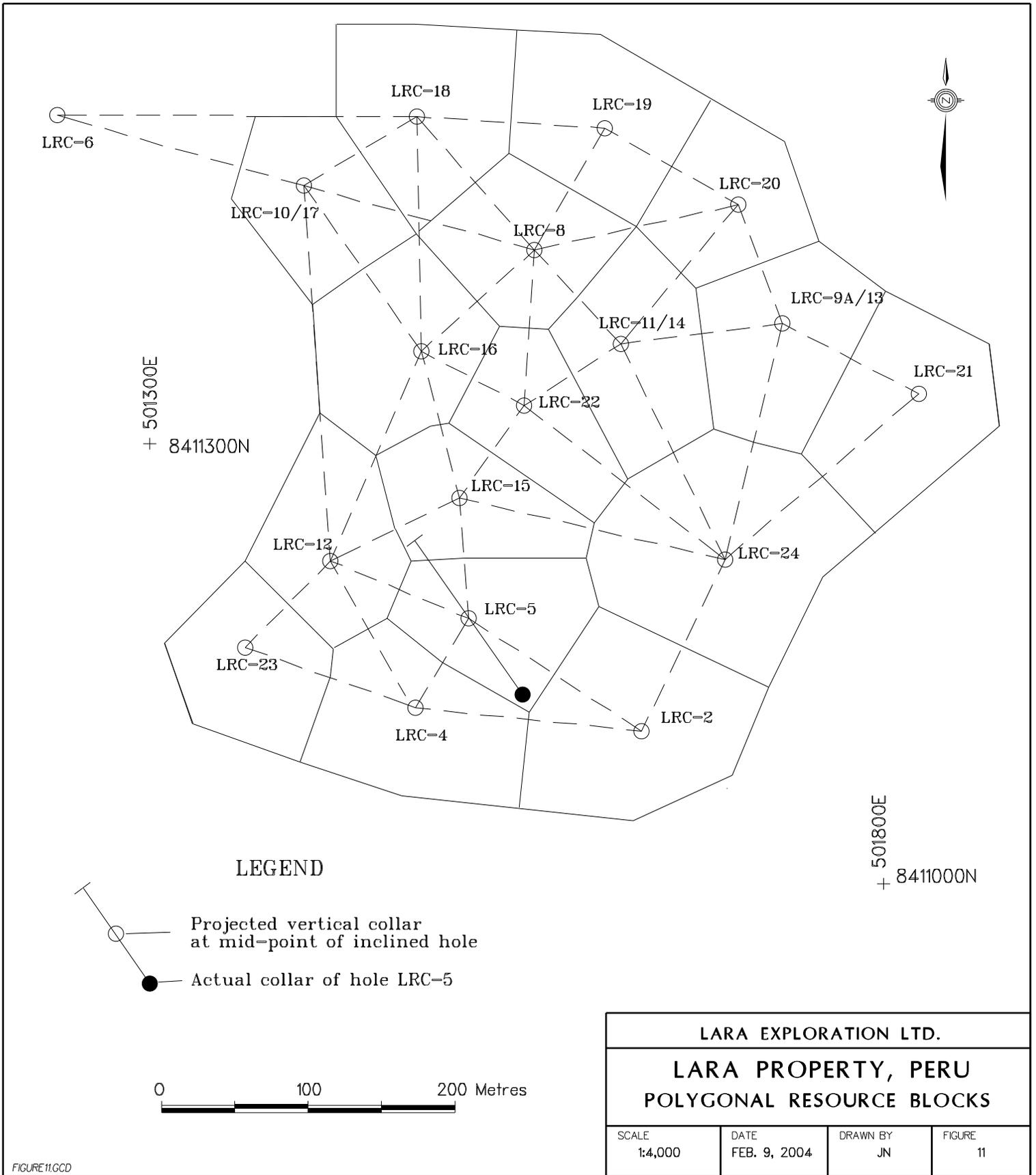
carbonates at the Lara property seems to range from minor to a large percentage of the total, as indicated in the analyses from the first twelve drill holes (see Appendix I.) The percentage of contained chalcocite has not yet been determined, but the metallurgical study conducted by Plenge Laboratories shows that the composite for LDD13 assayed 1.15% Cu when digested with NaCN, and LDD14 assayed 0.98% Cu. The total copper assays for these composites were 1.28% Cu and 1.23% Cu, respectively; this then indicates that about 90% of the copper minerals present are secondary sulphides, of which chalcocite is probably dominant (as ascertained by visiual inspection.)

The inferred resource data is presented in Tables 8 & 9, following.
An inferred resource of approximately 18.6 million tonnes grading 0.53% copper is determined using a 0.20% copper cut-off. Within this resource lies a smaller block of about 6.5 million tonnes grading 0.91% copper using a 0.50% copper cut-off and 4.8 million tonnes at 1.0% copper using a 0.60% copper cut-off (not shown in a table.) The most significant intercepts within the target area include: 28 meters of 1.2% copper in LDD-13; 24 meters of 1.2% copper in LDD-14; 16 meters of 1.1% copper in LRC-15; 14 meters of 1.2% copper in LRC-21 and 26 meters of 0.84% copper in LRC-22. Calculations of the above resources and intervals were carried to three significant figures but rounded off to two figures.

The zone seems to be truncated to the north and south but remains open to the east and west. Hole LRC-21 contains significant mineralization, and LRC-24, to the south, contains a moderate amount. To the west, hole LRC-23 contains a wide intercept of lower grade copper (64 meters at 0.38%) and LRC-12 contains 26 meters of 0.73% copper. The values in LRC-10 to the north are somewhat lower. An important fact to consider in further exploration to the west is that there exists a wide dyke swarm of various lithologies between LRC-16 and LRC-6. Much of this area is also underlain by the quartz porphyry/aplite unit. The dykes dip vertically to steeply west-northwest, and future drill programs in this area should be undertaken with angle holes only inclined to the east. Although some of the dykes appear barren, the dacite dykes, like the one encountered in LRC-16, scavenge copper and could contain a significant resource of lower grade copper.

Rescan Engineering, Vancouver, B.C., was commissioned to conduct a preliminary scoping study early in 1999. Their study, discussed later in detail, included a computerized resource estimate using Surpac software. Using horizontal sections at 100 m intervals, the mineral resource envelop was outlined using the upper and lower contacts of the mineralized zone (>0.2%Cu) and lithological contacts between rock types. The mineral resource envelop was then developed into a three dimensional solid model and subdivided into 20 m x 20 m x 10 m blocks.

Grades for individual blocks were estimated using the inverse distance to the second power method, a maximum search radius of 100 m, and a composited sample length of 10 m intervals. This resulted in a mineral inventory of 19.7 million tonnes grading 0.47% copper, using a 0.20% copper cut-off. Rescan Engineering has made no attempt to classify this resource as

Table 8. Inferred Resource (0.20% Copper Cut-Off)

Drillhole	Copper	Area	From	To	Interval	Volume	tonnage	tonnes	tonne x
	(0.2% cut-off)	(sq. metres)	(metres)	(metres)	(metres)	(cubic m)	factor		grade
LRC-2	0.44	16,307	0	20	20	326,140	2.6	847,964	373,104
LRC-2	0.22	16,307	26	28	2	32,614	2.6	84,796	18,655
LRC-2	0.46	16,307	42	68	26	423,982	2.6	1,102,353	507,082
LRC-4	0.54	13,036	28	70	42	547,512	2.6	1,423,531	768,707
LRC-5	0.56	10,065	18	38	20	201,300	2.6	523,380	293,093
LRC-8	0.48	10,050	42	50	8	80,400	2.6	209,040	100,339
LRC-8	0.2	10,050	58	60	2	20,100	2.6	52,260	10,452
LRC-8	0.37	10,050	62	72	10	100,500	2.6	261,300	96,681
LRC-9A	0.28	12,179	6	10	4	48,716	2.6	126,662	35,465
LRC-9A	0.33	12,179	14	16	2	24,358	2.6	63,331	20,899
LDD-13	0.95	12,179	74	110.6	36.6	445,751	2.6	1,158,954	1,101,006
LRC-10	0.51	9,811	62	86	24	235,464	2.6	612,206	312,225
LRC-11	0.29	11,575	52	58	6	69,450	2.6	180,570	52,365
LDD-14	1.08	11,575	69	97	28	324,100	2.6	842,660	910,073
LDD-14	0.38	11,575	100	108	8	92,600	2.6	240,760	91,489
LRC-12	0.38	10,482	8	24	16	167,712	2.6	436,051	165,699
LRC-12	0.51	10,482	36	100	64	670,848	2.6	1,744,205	889,544
LRC-15	0.61	9,145	58	102	44	402,380	2.6	1,046,188	638,175
LRC-16	0.45	12,353	36	46	10	123,530	2.6	321,178	144,530
LRC-16	0.2	12,353	64	66	2	24,706	2.6	64,236	12,847
LRC-16	0.29	12,353	82	90	8	98,824	2.6	256,942	74,513
LRC-19	0.22	11,844	30	32	2	23,688	2.6	61,589	13,550
LRC-19	0.59	11,844	36	52	16	189,504	2.6	492,710	290,699
LRC-20	0.35	9,412	22	38	16	150,592	2.6	391,539	137,039
LRC-21	0.37	12,923	36	40	4	51,692	2.6	134,399	49,728
LRC-21	0.32	12,923	58	62	4	51,692	2.6	134,399	43,008
LRC-21	0.74	12,923	78	114	36	465,228	2.6	1,209,593	895,099
LRC-22	0.68	8,578	84	120	36	308,808	2.6	802,901	545,973
LRC-23	0.38	9,756	26	90	64	624,384	2.6	1,623,398	616,891
LRC-24	0.21	20,998	20	22	2	41,996	2.6	109,190	22,930
LRC-24	0.23	20,998	30	32	2	41,996	2.6	109,190	25,114
LRC-24	0.25	20,998	36	46	10	209,980	2.6	545,948	136,487
LRC-24	0.21	20,998	49	50	1	20,998	2.6	54,595	11,465
LRC-24	0.32	20,998	59	62	3	62,994	2.6	163,784	52,411
LRC-24	0.39	20,998	64	69	5	104,990	2.6	272,974	106,460
LRC-24	0.21	20,998	71	72	1	20,998	2.6	54,595	11,465
LRC-24	0.42	20,998	73	86	13	272,974	2.6	709,732	298,088
LRC-24	0.23	20,998	88	89.7	1.7	35,697	2.6	92,811	21,347
TOTALS:						7,139,198		18,561,915	9,894,696
GRADE:	0.53%	(0.20% CUT-OFF)							
TONNES	18,561,914.80	(rounded to 18.6 million tonnes)							

Table 9. Inferred Resource (0.50% Copper Cut-Off)

Drillhole	Copper	Area	From	To	Interval	Volume	tonnage	tonnes	tonnes x
	(0.5% cut-off)	(sq. metres)	(metres)	(metres)	(metres)	(cubic m)	factor		grade
LRC-2	0.68	16,307	48	50	2	32,614	2.6	84,796	57,662
LRC-2	1.14	16,307	54	56	2	32,614	2.6	84,796	96,668
LRC-2	0.6	16,307	62	64	2	32,614	2.6	84,796	50,878
LRC-4	1.2	13,036	50	56	6	78,216	2.6	203,362	244,034
LRC-4	1.39	13,036	64	68	4	52,144	2.6	135,574	188,448
LRC-5	0.62	10,065	18	26	8	80,520	2.6	209,352	129,798
LRC-5	0.56	10,065	30	38	8	80,520	2.6	209,352	117,237
LRC-8	0.69	10,050	42	44	2	20,100	2.6	52,260	36,059
LRC-8	0.66	10,050	68	72	4	40,200	2.6	104,520	68,983
LDD-13	1.15	12,179	75	103	28	341,012	2.6	886,631	1,019,626
LRC-10	0.55	9,811	64	68	4	39,244	2.6	102,034	56,119
LRC-10	0.65	9,811	70	72	2	19,622	2.6	51,017	33,161
LRC-10	0.62	9,811	74	82	8	78,488	2.6	204,069	126,523
LDD-14	1.21	11,575	72	96	24	277,800	2.6	722,280	873,959
LDD-14	0.55	11,575	100	101	1	11,575	2.6	30,095	16,552
LDD-14	0.74	11,575	102	104	2	23,150	2.6	60,190	44,541
LRC-12	1.02	10,487	20	22	2	20,974	2.6	54,532	55,623
LRC-12	0.55	10,487	44	48	4	41,948	2.6	109,065	59,986
LRC-12	0.7	10,487	52	54	2	20,974	2.6	54,532	38,173
LRC-12	0.73	10,487	64	90	26	272,662	2.6	708,921	517,512
LRC-15	1.12	9,145	58	74	16	146,320	2.6	380,432	426,084
LRC-15	0.56	9,145	88	90	2	18,290	2.6	47,554	26,630
LRC-16	0.55	12,353	42	44	2	24,706	2.6	64,236	35,330
LRC-19	0.86	11,844	40	48	8	94,752	2.6	246,355	211,865
LRC-21	1.23	12,923	78	92	14	180,922	2.6	470,397	578,589
LRC-21	0.53	12,923	104	106	2	25,846	2.6	67,200	35,616
LRC-21	0.76	12,923	108	110	2	25,846	2.6	67,200	51,072
LRC-22	0.84	8,578	84	110	26	223,028	2.6	579,873	487,093
LRC-23	0.56	9,756	54	56	2	19,512	2.6	50,731	28,409
LRC-23	0.51	9,756	58	60	2	19,512	2.6	50,731	25,873
LRC-23	0.59	9,756	64	66	2	19,512	2.6	50,731	29,931
LRC-24	0.55	20,998	65	67	2	41,996	2.6	109,190	60,054
LRC-24	0.59	20,998	81	86	5	104,990	2.6	272,974	161,055
TOTALS:						2,509,609		6,524,983	5,931,481
GRADE:	0.91%	(0.50% CUT-OFF)							
TONNES	6,524,983.40	(rounded to 6.5 million tonnes)							

measured, indicated or inferred, but refer to their estimate as a mineral inventory. The author has opted to classify Rescan's estimation as an "inferred resource."

Both methods used by the author and by Rescan Engineering are believed to be accurate, relevant and in accordance with methods that comply with NI 43-101 standards.

Table 10. Comparison of Calculated Inferred Mineral Resources

Calculation	Inferred Resources (tonnes)	Grade (% Cu)	Contained Copper (tonnes)
PGS	18,562,000	0.53	98,378
Hatch/Rescan Eng.	19,749,600	0.47	93,219
Variance			-5.24%

Interpretations and Conclusions

Mapping, surface sampling and induced polarization surveys have defined a porphyry copper target over an area of 6 km^2 on the Lara 2A and Lara 4 claims.

Three drilling programs by the Company have outlined copper mineralization over an area 500 meters north-south by 500 meters east-west which is open to the east and west. Chalcocite was observed as fine grains and as coatings on finely disseminated pyrite and chalcopyrite. The supergene zone starts, on average, about 60 to 80 meters below surface and ranges from 20 to 40 meters in thickness. An in-situ mineral inventory of 18.6 million tonnes at 0.53% copper (0.20% cut-off), 6.5 million tonnes at 0.91% copper (0.50% cut-off) and 4.8 million tonnes at 1.04% copper (0.60% cut-off) was manually calculated by the author using the polygonal block method. No kriging or other geostatistical check was performed on this estimate, but the inventory has been classified by the author as an *inferred resource*.

Rescan Engineering calculated an inferred mineral resource of approximately 19.75 million tonnes grading 0.47% copper, using a 0.20% copper cut-off. Their estimate was generated using Surpac software and employing the inverse distance squared technique. Rescan has chosen not to classify the resource in any category but refer to it as a mineral inventory, until further in-fill drilling results provide sufficient data for analysis by geostatistical methods. Both methods used by the author and by Rescan Engineering are believed to be accurate, relevant and in accordance with methods that comply with NI 43-101 standards.

Potential to increase the tonnage of the deposit lies to the east and west and possibly to the south; early drill results suggest that potentially economic mineralization may already be delimited to the north of the main Lara zone. Mapping and sampling done between 1997 and 1999 in the Mina de Socos zone suggests that the Lara porphyry system extends to here, at least 800 meters east of the area drilled so far.

The column leach study performed on drill core for two different holes (LDD13 and LDD14) yielded copper extractions of 90.6% and 87.1% over 161 days and 154 days, respectively. These recoveries indicate that the secondary sulphides are quite amenable to SX/EW heap leach extraction methods.

Recommendations

Due to the strong copper price at this time, the Issuer has requested the author to propose a revised exploration program and budget that could adequately test the Lara deposit for the additional tonnes required to make the deposit potentially economic. A program similar to the one outlined by the author in his 2001 report for Peruvian Gold Limited is proposed.

A 3,000 metres combined reverse circulation and diamond drilling program should be performed to test the extent of the Lara/Socos porphyry system. A total of twenty-five holes are proposed, all of which are located east of the existing drilling up to and including the Mina de Socos zone. These holes are all vertical and will be open-holed (not sampled) using R.C. drilling in the leached cap, followed by HQ diameter diamond drilling as the supergene zone is approached. The site geologist(s) will have to determine the appropriateness of this method and probably shorten the R.C. interval in new areas until a better understanding of the supergene zone's geometry, if present, is understood.

The first phase program is focused on drilling holes immediately west of Mina de Socos to test the mineral potential of the highly leached porphyry that subcrops here. The remaining holes would infill the area between Mina de Socos and the main Lara porphyry body. Some additional holes should be located west of the main Lara body at the Issuer's discretion. The drilling program should cost about US$436,300, or CDN$523.560.

Rescan Engineering has recommended additional drilling to find sufficient resources, as those assumed in their study. In addition, they propose further integrated geological/metallurgical evaluations, geostatistical analyses, resource classification by a professional economic geologist, pit optimization, preliminary environmental assessments and site inspections for heap leach pads, process plant, pond and waste sites. It is the author's opinion that these recommendations are totally dependant upon success in delineating the additional resources Rescan estimated are needed to make Lara a potentially economic deposit. Therefore, no budget for the above-mentioned recommendations is proposed at this time.

_____
John Nebocat, P. Eng.
Gibsons, B.C.
March 31, 2005

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Statement of Qualifications

I, John Nebocat, residing at 1486 Island View Drive, Gibsons, British Columbia, declare that:

1. I am a geologist and "qualified person" and have been employed in mineral exploration and earth science studies with industry and government since 1973.

2. I obtained a diploma in Mining Technology from the British Columbia Institute of Technology in 1974. In 1984, I graduated from the Montana College of Mineral Science & Technology with a Bachelor's Degree in Geological Engineering (Honours).

3. I am a registered Professional Engineer with the Association of Professional Engineers and Geoscientists of British Columbia (1986.)

4. I visited the Lara property for four days 1995, for one week in 1997, for about ten days in 1998 and one day in 1999, performing geologic mapping, sampling and a review of the first two drilling programs. I supervised the third drilling program.

5. I am independent of the Issuer. I do not own nor will I receive any interest, either direct or indirect, in the properties described herein., nor do I own an interest in the securities of Quest Investment Corporation, Lara Exploration Ltd., or any of their affiliates.

6. I am responsible for the compilation of all parts of this report.

7. I am not aware of any material fact or material change with respect to the subject matter contained within this technical report that would cause it to be misleading.

8. I have read Intsrument 43-101 amd Form 43-101F1; this report has been prepared in accordance with the guidelines of the aforementioned instrument and form.

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John Nebocat, B.Sc., P. Eng.

Appendix I

Summary of Analyses

From Drilling Programs

Lara Project, Peru

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-1	0	2	6001	160			53		5				2	
LRC-1	2	4	6002	200			56		7				2	
LRC-1	4	6	6003	156			38		5				2	
LRC-1	6	8	6004	224			50		6				2	
LRC-1	8	10	6005	265			87		5				2	
LRC-1	10	12	6006	1850			575		3				2	
LRC-1	12	14	6007	910			215		84				2	
LRC-1	14	16	6008	1120			268		20				2	
LRC-1	16	18	6009	1050			250		29				2	
LRC-1	18	20	6010	650			190		45	697			2	
LRC-1	20	22	6011	1060			420		69				2	
LRC-1	22	24	6012	1980			990		12				2	
LRC-1	24	26	6013	1900			870		11				2	
LRC-1	26	28	6014	1290			562.5		5				2	
LRC-1	28	30	6016	1180			600		18				2	
LRC-1	30	32	6017	1360			530		13				2	
LRC-1	32	34	6018	850			160		14				2	
LRC-1	34	36	6019	880			95		55				2	
LRC-1	36	38	6020	1000			190		20				2	
LRC-1	38	40	6021	600			100		29				2	
LRC-1	40	42	6022	1285			140		64				2	
LRC-1	42	44	6023	880			45		25				2	
LRC-1	44	46	6024	815			80		24				2	
LRC-1	46	48	6025	735			30		8				2	
LRC-1	48	50	6026	665			20		28				2	
LRC-1	50	52	6027	620			30		30	707			2	
LRC-1	52	54	6028	580			20		15				2	
LRC-1	54	56	6029	860			30		10				2	
LRC-1	56	58	6030	640			16		12				2	
LRC-1	58	60	6031	1080			18		25				2	
LRC-1	60	62	6032	850			55		12				2	
LRC-1	62	64	6033	1040			51		48				2	
LRC-1	64	66	6034	1600			46		47				2	
LRC-1	66	68	6035	870			45		24				2	
LRC-1	68	70	6036	650			40		23				2	
LRC-1	70	72	6037	960			30		24	1155			2	
LRC-1	72	74	6038	910			44		15				2	
LRC-1	74	76	6039	830			46		28				2	
LRC-1	76	78	6040	1070			20		42				2	
LRC-1	78	80	6041	780			28		31				2	
LRC-1	80	82	6042	670			17		18				2	
LRC-1	82	84	6043	530			10		24				2	
LRC-1	84	86	6044	460			26		32				2	
LRC-1	86	88	6045	660			5		45				2	
LRC-1	88	90	6046	300			27		31				2	
LRC-1	90	92	6047	380			47		33	741			2	
LRC-1	92	94	6048	1320			50		26				2	
LRC-1	94	96	6049	835			13		10				2	
LRC-1	96	98	6050	628			33		5				2	
LRC-1	98	100	6051	550			15		9				2	
LRC-1	100	102	6052	800			16		15				2	
LRC-1	102	104	6053	790			27		88				2	
LRC-1	104	106	6054	1060			33		123				2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-1	106	108	6055	700			23		54				2	
LRC-1	108	110	6056	1500			45		14				2	
LRC-1	110	112	6057	1200			30		9	1428			2	
LRC-1	112	114	6058	990			17		10				2	
LRC-1	114	116	6059	710			24		47				2	
LRC-1	116	118	6060	760			8		26				2	
LRC-1	118	120	6061	460			10		105				2	
LRC-1	120	122	6062	520			20		18				2	
LRC-1	122	124	6063	570			25		62				2	
LRC-1	124	126	6064	500			27		12				2	
LRC-1	126	128	6065	550			26		15				2	
LRC-1	128	130	6066	600			14		8				2	
LRC-1	130	132	6067	600			67		40	1346			2	
LRC-1	132	134	6068	1080			18		27				2	
LRC-1	134	136	6069	660			32		14				2	
LRC-1	136	137	6070	1050			24		58				2	
LRC-2	0	2	6071	3900			1470		20				2	
LRC-2	2	4	6072	3600			1990		27				2	
LRC-2	4	6	6073	4100			2550		17				2	
LRC-2	6	8	6074	3200			1800		18				2	
LRC-2	8	10	6075	4900			2500		25				2	
LRC-2	10	12	6076	3900			1800		20				2	
LRC-2	12	14	6077	6500			4650		37	6077			2	
LRC-2	14	16	6078	7500			5200		21				2	
LRC-2	16	18	6079	3600			1560		80				2	
LRC-2	18	20	6080	3100			1450		67			0.44%	2	20
LRC-2	20	22	6081	1850			930		21				2	
LRC-2	22	24	6082	1750			830		40				2	
LRC-2	24	26	6083	1570			775		25				2	
LRC-2	26	28	6084	2200			1325		22			0.22%	2	2
LRC-2	28	30	6085	1400			710		39				2	
LRC-2	30	32	6086	1400			585		90				2	
LRC-2	32	34	6087	1000			400		35				2	
LRC-2	34	36	6088	840			220		120	875			2	
LRC-2	36	38	6089	740			250		82				2	
LRC-2	38	40	6090	1155			535		60				2	
LRC-2	40	42	6091	1500			890		58				2	
LRC-2	42	44	6092	3090			1995		71				2	
LRC-2	44	46	6093	1800			1150		81				2	
LRC-2	46	48	6094	2900			1660		89				2	
LRC-2	48	50	6095	6800			3200		56				2	2
LRC-2	50	52	6096	3900			740		49				2	
LRC-2	52	54	6097	4000			610		22				2	
LRC-2	54	56	6098	11400			615		26	10758			2	2
LRC-2	56	58	6099	4700			1280		78				2	
LRC-2	58	60	6100	4375			940		36				2	
LRC-2	60	62	6101	3200			345		74				2	
LRC-2	62	64	6102	6000			1050		40				2	2
LRC-2	64	66	6103	4200			670		96				2	
LRC-2	66	68	6104	2900			260		38			0.46%	2	26
LRC-2	68	70	6105	880			440		17				2	
LRC-2	70	72	6106	380			60		10				2	
LRC-2	72	74	6107	750			39		15				2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-2	74	76	6108	410			20		20				2	
LRC-2	76	78	6109	490			35		21				2	
LRC-2	78	80	6110	385			30		3	434			2	
LRC-2	80	82	6111	1780			48		2				2	
LRC-2	82	84	6112	477			20		2				2	
LRC-2	84	86	6113	880			16		2				2	
LRC-2	86	88	6114	441			10		3				2	
LRC-2	88	90	6115	1540			33		2				2	
LRC-2	90	92	6116	1000			48		16				2	
LRC-2	92	94	6117	1240			36		18				2	
LRC-2	94	96	6118	1550			30		30				2	
LRC-2	96	98	6119	1670			20		40				2	
LRC-2	98	100	6120	1250			13		28	1458			2	
LRC-2	100	102	6121	1159			10		39				2	
LRC-2	102	104	6122	3100			29		41				2	
LRC-2	104	106	6123	680			8		37				2	
LRC-2	106	108	6124	1525			10		24				2	
LRC-2	108	110	6125	2900			30		24				2	
LRC-2	110	112	6126	1300			16		48				2	
LRC-2	112	114	6127	190			24		6				2	
LRC-2	114	116	6128	610			20		7				2	
LRC-2	116	118	6129	1450			42		28				2	
LRC-2	118	120	6130	820			30		30	888			2	
LRC-2	120	122	6131	960			35		31				2	
LRC-2	122	124	6132	970			32		26				2	
LRC-2	124	126	6133	1200			40		14				2	
LRC-2	126	128	6134	3300			49		29				2	
LRC-2	128	130	6135	2700			48		22				2	
LRC-2	130	132	6136	2200			54		18				2	
LRC-2	132	134	6137	1350			30		21				2	
LRC-2	134	136	6138	1900			50		52				2	
LRC-2	136	138	6139	2100			34		21				2	
LRC-2	138	140	6140	2900			31		11	2789			2	
LRC-2	140	142	6141	1700			27		22				2	
LRC-2	142	144	6142	620			20		18				2	
LRC-2	144	146	6143	900			19		13				2	
LRC-2	146	148	6144	1300			13		23				2	
LRC-2	148	150	6145	940			18		18				2	
LRC-2	150	152	6146	730			20		16				2	
LRC-2	152	154	6147	1600			26		12				2	
LRC-2	154	156	6148	1800			35		23				2	
LRC-2	156	158	6149	720			10		11				2	
LRC-2	158	160	6150	1500			28		13	1635			2	
LRC-2	160	162	6151	1600			16		23				2	
LRC-2	162	164	6152	600			18		5				2	
LRC-2	164	166	6153	650			28		13				2	
LRC-2	166	168	6154	1230			24		14				2	
LRC-2	168	170	6155	1000			30		9				2	
LRC-2	170	172	6156	400			10		7				2	
LRC-2	172	174	6157	480			5		12				2	
LRC-2	174	176	6158	1900			23		18				2	
LRC-2	176	178	6159	247			8		12				2	
LRC-2	178	180	6160	660			7		4	819			2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-2	180	182	6161	660			17		5				2	
LRC-2	182	184	6162	755			20		14				2	
LRC-2	184	186	6163	1400			31		9				2	
LRC-2	186	188	6164	1200			28		20				2	
LRC-2	188	190	6165	1000			37		6				2	
LRC-2	190	192	6166	665			26		11				2	
LRC-2	192	194	6167	2100			82		5				2	
LRC-2	194	196	6168	425			23		8				2	
LRC-2	196	198	6169	480			29		4				2	
LRC-2	198	200	6170	455			26		5	653			2	
LRC-2	200	202	6171	1300			76		21				2	
LRC-2	202	204	6172	800			58		7				2	
LRC-2	204	206	6173	365			19		7				2	
LRC-2	206	208	6174	790			47		8				2	
LRC-2	208	210	6175	1400			96		13				2	
LRC-2	210	212	6176	1000			57		9				2	
LRC-3	0	2	6177	1130			369		11				2	
LRC-3	2	4	6178	1260			367		13				2	
LRC-3	4	6	6179	1350			420		12				2	
LRC-3	6	8	6180	860			222		8				2	
LRC-3	8	10	6181	450			126		5				2	
LRC-3	10	12	6182	700			327		8				2	
LRC-3	12	14	6183	240			69		4				2	
LRC-3	14	16	6184	190			60		5				2	
LRC-3	16	18	6185	260			83		8				2	
LRC-3	18	20	6186	300			95		6	334			2	
LRC-3	20	22	6187	470			175		5				2	
LRC-3	22	24	6188	950			374		5				2	
LRC-3	24	26	6189	1350			475		31				2	
LRC-3	26	28	6190	270			80		11				2	
LRC-3	28	30	6191	640			166		17				2	
LRC-3	30	32	6192	660			165		34				2	
LRC-3	32	34	6193	980			242		22				2	
LRC-3	34	36	6194	1500			392		105				2	
LRC-3	36	38	6195	1750			480		67				2	
LRC-3	38	40	6196	2100			613		32				2	
LRC-3	40	42	6197	3500			1375		13				2	
LRC-3	42	44	6198	2950			1000		134	2933			2	
LRC-3	44	46	6199	3400			1225		184				2	
LRC-3	46	48	6200	3100			1336		120				2	
LRC-3	48	50	6201	3300			1128		59				2	
LRC-3	50	52	6202	3400			1045		39			0.31%	2	14
LRC-3	52	54	6203	1150			300		41				2	
LRC-3	54	56	6204	770			267		81				2	
LRC-3	56	58	6205	1750			945		30				2	
LRC-3	58	60	6206	3000			1750		25				2	
LRC-3	60	62	6207	4100			1700		39				2	
LRC-3	62	64	6208	2190			1350		43	4116			2	
LRC-3	64	66	6209	2500			490		63				2	
LRC-3	66	68	6210	6425			928		44				2	
LRC-3	68	70	6211	6000			880		54			0.62%	2	4
LRC-3	70	72	6212	2900			480		99				2	
LRC-3	72	74	6213	3000			466		211				2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-3	74	76	6214	2700			200		60				2	
LRC-3	76	78	6215	3800			195		98				2	
LRC-3	78	80	6216	2900			190		63				2	
LRC-3	80	82	6217	2400			157		64				2	
LRC-3	82	84	6218	2500			128		40	2552		0.34%	2	26
LRC-3	84	86	6219	1500			159		50				2	
LRC-3	86	88	6220	2400			350		52			0.24%	2	2
LRC-3	88	90	6221	1800			230		70				2	
LRC-3	90	92	6222	2300			314		51			0.23%	2	2
LRC-3	92	94	6223	1700			160		105				2	
LRC-3	94	96	6224	2650			182		85				2	
LRC-3	96	98	6225	2300			131		78				2	
LRC-3	98	100	6226	2400			92		45				2	
LRC-3	100	102	6227	2400			78		84				2	
LRC-3	102	104	6228	2900			181		83	2863			2	
LRC-3	104	106	6229	1900			164		54				2	
LRC-3	106	108	6230	3200			92		124				2	
LRC-3	108	110	6231	2500			104		40				2	
LRC-3	110	112	6232	3000			149		50				2	
LRC-3	112	114	6233	2550			140		147				2	
LRC-3	114	116	6234	3300			390		71				2	
LRC-3	116	118	6235	3100			300		57				2	
LRC-3	118	120	6236	2000			157		56				2	
LRC-3	120	122	6237	2700			323		66				2	
LRC-3	122	124	6238	3800			415		48	2882			2	
LRC-3	124	126	6239	2850			673		30				2	
LRC-3	126	128	6240	2700			530		78				2	
LRC-3	128	130	6241	3600			576		146				2	
LRC-3	130	132	6242	2650			506		160				2	
LRC-3	132	134	6243	3600			964		42				2	
LRC-3	134	136	6244	2700			555		28				2	
LRC-3	136	138	6245	2860			310		79				2	
LRC-3	138	140	6246	2400			560		82				2	
LRC-3	140	142	6247	2500			320		235				2	
LRC-3	142	144	6248	3950			363		91	4181			2	
LRC-3	144	146	6249	3300			395		38				2	
LRC-3	146	148	6250	2600			190		68			0.28%	2	54
LRC-3	148	150	6251	1980			160		475				2	
LRC-3	150	152	6252	1400			124		312				2	
LRC-3	152	154	6253	1400			97		300				2	
LRC-3	154	156	6254	3100			162		2660				2	
LRC-3	156	158	6255	2350			157		267			0.27%	2	4
LRC-3	158	160	6256	1200			81		198				2	
LRC-3	160	162	6257	2000			75		110				2	
LRC-3	162	164	6258	2650			130		60	2748			2	
LRC-3	164	166	6259	2600			145		30			0.24%	2	6
LRC-3	166	168	6260	1825			110		64				2	
LRC-4	0	2	6261	670			233		5				2	
LRC-4	2	4	6262	1050			275		3				2	
LRC-4	4	6	6263	450			118		10				2	
LRC-4	6	8	6264	430			139		14				2	
LRC-4	8	10	6265	420			137		6				2	
LRC-4	10	12	6266	695			230		7				2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-4	12	14	6267	870			340		8				2	
LRC-4	14	16	6268	1080			815		4				2	
LRC-4	16	18	6269	1170			1160		ND				2	
LRC-4	18	20	6270	1500			1430		ND	1785			2	
LRC-4	20	22	6271	1340			1320		ND				2	
LRC-4	22	24	6272	810			760		3				2	
LRC-4	24	26	6273	1640			1620		2				2	
LRC-4	26	28	6274	1620			1580		2				2	
LRC-4	28	30	6275	2000			1990		2				2	
LRC-4	30	32	6276	4700			4150		3				2	
LRC-4	32	34	6277	4400			3920		2				2	
LRC-4	34	36	6278	4450			3840		3				2	
LRC-4	36	38	6279	4100			3400		3				2	
LRC-4	38	40	6280	3560			3000		3	4482			2	
LRC-4	40	42	6281	3200			2470		4				2	
LRC-4	42	44	6282	2100			1680		2				2	
LRC-4	44	46	6283	2900			2200		2				2	
LRC-4	46	48	6284	1650			1200		2				2	
LRC-4	48	50	6285	2150			1700		2				2	
LRC-4	50	52	6286	10000			8800		3				2	
LRC-4	52	54	6287	12100			10450		2				2	
LRC-4	54	56	6288	13900			13360		8			1.20%	2	6
LRC-4	56	58	6289	4300			3450		2				2	
LRC-4	58	60	6290	1600			1440		9	1677			2	
LRC-4	60	62	6291	2600			2190		3				2	
LRC-4	62	64	6292	2480			2200		2				2	
LRC-4	64	66	6293	8250			6660		3				2	
LRC-4	66	68	6294	19600			17600		6			1.39%	2	4
LRC-4	68	70	6295	3500			3100		5				2	42
LRC-4	70	72	6296	239			230		2			0.54%	2	
LRC-4	72	74	6297	460			454		6				2	
LRC-4	74	76	6298	1800			1670		5				2	
LRC-4	76	78	6299	53			60		2				2	
LRC-4	78	80	6300	380			375		3	444			2	
LRC-4	80	82	6301	620			616		ND				2	
LRC-4	82	84	6302	716			696		ND				2	
LRC-4	84	86	6303	395			383		ND				2	
LRC-4	86	88	6304	1400			1385		ND				2	
LRC-4	88	90	6305	120			83		ND				2	
LRC-4	90	92	6306	160			106		ND	192			2	
LRC-4	92	94	6307	210			142		ND				2	
LRC-4	94	96	6308	254			133		ND				2	
LRC-4	96	98	6309	376			340		ND				2	
LRC-4	98	100	6310	150			107		ND				2	
LRC-4	100	102	6311	135			63		ND				2	
LRC-4	102	104	6312	122			33		ND				2	
LRC-4	104	106	6313	30			26		ND				2	
LRC-4	106	108	6314	55			15		ND				2	
LRC-4	108	110	6315	129			30		ND				2	
LRC-4	110	112	6316	125			67		ND	141			2	
LRC-4	112	114	6317	184			86		ND				2	
LRC-4	114	116	6318	55			22		ND				2	
LRC-4	116	118	6319	67			28		ND				2	

The original results from Plenge Laboratories are used in the composite calculations

Appendix I: Summary of Analyses From Drilling Programs, Lara Project, Peru

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-4	118	120	6320	36			18		ND				2	
LRC-4	120	122	6321	16			12		ND				2	
LRC-4	122	124	6322	31			12		ND				2	
LRC-4	124	126	6323	22			7		ND				2	
LRC-4	126	128	6324	142			20		2				2	
LRC-4	128	130	6325	545			30		ND				2	
LRC-4	130	132	6326	1700			79		4	2194			2	
LRC-4	132	134	6327	2100			68		54				2	
LRC-4	134	136	6328	1800			55		82				2	
LRC-4	136	138	6329	2600			78		25				2	
LRC-4	138	140	6330	2800			76		45				2	
LRC-4	140	142	6331	2400			66		37				2	
LRC-4	142	144	6332	2400			90		18				2	
LRC-4	144	146	6333	2900			93		14				2	
LRC-4	146	148	6334	2600			82		36				2	
LRC-4	148	150	6335	2300			56		32				2	
LRC-4	150	152	6336	2800			73		27	3515			2	
LRC-4	152	154	6337	2600			65		23				2	
LRC-4	154	156	6338	2700			84		39				2	
LRC-4	156	158	6339	2500			75		28				2	
LRC-4	158	160	6340	2800			93		44				2	
LRC-4	160	162	6341	2600			73		15				2	
LRC-4	162	164	6342	3400			86		26				2	
LRC-4	164	166	6343	2700			75		35				2	
LRC-4	166	168	6344	2900			86		57				2	
LRC-4	168	170	6345	1800			56		60				2	
LRC-4	170	172	6346	1600			46		48	1809			2	
LRC-4	172	174	6347	1600			54		14				2	
LRC-4	174	176	6348	1600			55		9				2	
LRC-4	176	178	6349	1500			46		15				2	
LRC-4	178	180	6350	1800			59		40				2	
LRC-4	180	182	6351	2200			53		20				2	
LRC-4	182	184	6352	3000			81		10				2	
LRC-4	184	186	6353	3400			108		20				2	
LRC-4	186	188	6354	3300			116		10				2	
LRC-4	188	190	6355	3900			123		17				2	
LRC-4	190	192	6356	3000			90		27	3679			2	
LRC-4	192	194	6357	2700			67		29				2	
LRC-4	194	196	6358	2400			71		11				2	
LRC-4	196	198	6359	2200			60		22				2	
LRC-4	198	200	6360	1800			54		13				2	
LRC-4	200	202	6361	1400			52		22				2	
LRC-4	202	204	6362	2000			73		16				2	
LRC-4	204	206	6363	1600			49		27				2	
LRC-4	206	208	6364	1700			53		16				2	
LRC-4	208	210	6365	2500			81		15				2	
LRC-4	210	212	6366	2100			56		29	2487			2	
LRC-4	212	214	6367	615			22		6				2	
LRC-4	214	216	6368	70			4		ND				2	
LRC-4	216	218	6369	155			12		2				2	
LRC-4	218	220	6370	154			13		2				2	
LRC-4	220	222	6371	29			4		ND				2	
LRC-5	0	2	6372	880			216		170				2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-5	2	4	6373	710			200		127				2	
LRC-5	4	6	6374	860			271		100				2	
LRC-5	6	8	6375	780			262		120				2	
LRC-5	8	10	6376	740			280		162				2	
LRC-5	10	12	6377	1165			555		76				2	
LRC-5	12	14	6378	1190			848		44				2	
LRC-5	14	16	6379	1340			810		33				2	
LRC-5	16	18	6380	1000			720		73				2	
LRC-5	18	20	6381	5000			1950		17	5372			2	
LRC-5	20	22	6382	7400			1800		31				2	
LRC-5	22	24	6383	6200			1960		90				2	
LRC-5	24	26	6384	6350			1630		113			0.62%	2	8
LRC-5	26	28	6385	3600			1215		32				2	
LRC-5	28	30	6386	4600			1210		46				2	
LRC-5	30	32	6387	5000			1020		49				2	
LRC-5	32	34	6388	5700			1660		58				2	
LRC-5	34	36	6389	5500			1700		20			0.56%	2	8
LRC-5	36	38	6390	6200			2120		40			0.56%	2	20
LRC-5	38	40	6391	1820			280		36	2187			2	
LRC-5	40	42	6392	1000			135		28				2	
LRC-5	42	44	6393	1200			270		48				2	
LRC-5	44	46	6394	1400			110		55				2	
LRC-5	46	48	6395	1650			196		53				2	
LRC-5	48	50	6396	1950			188		66				2	
LRC-5	50	52	6397	1700			134		84				2	
LRC-5	52	54	6398	1850			140		137				2	
LRC-5	54	56	6399	1760			325		130				2	
LRC-5	56	58	6400	1640			264		39				2	
LRC-5	58	60	6401	2600			330		20	2730			2	
LRC-5	60	62	6402	1850			305		27				2	
LRC-5	62	64	6403	3000			850		150				2	
LRC-5	64	66	6404	1600			320		61				2	
LRC-5	66	68	6405	1390			130		25				2	
LRC-5	68	70	6406	1420			100		7				2	
LRC-5	70	72	6407	860			99		10				2	
LRC-5	72	74	6408	1000			97		11				2	
LRC-5	74	76	6409	1000			95		18				2	
LRC-5	76	78	6410	1160			293		72				2	
LRC-5	78	80	6411	4200			580		66	4482			2	
LRC-5	80	82	6412	1900			280		68				2	
LRC-5	82	84	6413	1500			86		55				2	
LRC-5	84	86	6414	3200			160		105				2	
LRC-5	86	88	6415	4000			209		210				2	
LRC-5	88	90	6416	880			175		31	1005			2	
LRC-5	90	92	6417	1800			251		50				2	
LRC-5	92	94	6418	2300			220		62				2	
LRC-5	94	96	6419	1000			64		22				2	
LRC-5	96	98	6420	768			72		19				2	
LRC-5	98	100	6421	575			38		19				2	
LRC-5	100	102	6422	646			24		23				2	
LRC-5	102	104	6423	2200			42		75				2	
LRC-5	104	106	6424	2000			69		32				2	
LRC-5	106	108	6425	1800			68		41				2	

The original results from Plenge Laboratories are used in the composite calculations

Appendix I: Summary of Analyses From Drilling Programs, Lara Project, Peru

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-5	108	110	6426	1600			70		36	1902			2	
LRC-5	110	112	6427	1600			74		64				2	
LRC-5	112	114	6428	1400			89		53				2	
LRC-5	114	116	6429	760			22		106				2	
LRC-5	116	118	6430	1625			65		140				2	
LRC-5	118	120	6431	1900			68		130				2	
LRC-5	120	122	6432	2100			94		102				2	
LRC-5	122	124	6433	2800			166		35				2	
LRC-5	124	126	6434	2700			145		25				2	
LRC-5	126	128	6435	1600			94		48				2	
LRC-5	128	130	6436	2800			153		63	2987			2	
LRC-5	130	132	6437	3200			187		77				2	
LRC-5	132	134	6438	2600			120		54				2	
LRC-5	134	136	6439	2800			160		80				2	
LRC-5	136	138	6440	2700			139		34				2	
LRC-5	138	140	6441	2600			130		40				2	
LRC-5	140	142	6442	950			83		15				2	
LRC-5	142	144	6443	1400			90		8				2	
LRC-5	144	146	6444	1265			70		8				2	
LRC-5	146	148	6445	2000			85		46				2	
LRC-5	148	150	6446	1900			68		107	2118			2	
LRC-5	150	152	6447	1200			72		11				2	
LRC-5	152	154	6448	600			57		10				2	
LRC-5	154	156	6449	2100			80		80				2	
LRC-5	156	158	6450	3400			102		64				2	
LRC-5	158	160	6451	2900			100		45				2	
LRC-5	160	162	6452	3000			98		56				2	
LRC-5	162	164	6453	1600			77		25				2	
LRC-5	164	166	6454	1350			85		29				2	
LRC-5	166	168	6455	1000			57		10				2	
LRC-5	168	170	6456	805			44		5	937			2	
LRC-5	170	172	6457	725			46		4				2	
LRC-5	172	174	6458	840			47		12				2	
LRC-5	174	176	6459	850			39		8				2	
LRC-5	176	178	6460	1400			66		6				2	
LRC-5	178	180	6461	1600			64		55				2	
LRC-5	180	182	6462	1600			100		53				2	
LRC-5	182	184	6463	2200			138		24				2	
LRC-5	184	186	6464	2400			148		6				2	
LRC-5	186	188	6465	1800			65		66				2	
LRC-5	188	190	6466	2200			93		45	2470			2	
LRC-5	190	192	6467	1700			96		55				2	
LRC-5	192	194	6468	1563			60		73				2	
LRC-5	194	196	6469	2000			110		40				2	
LRC-5	196	198	6470	1400			102		26				2	
LRC-5	198	200	6471	1800			31		43				2	
LRC-5	200	202	6472	760			2		27				2	
LRC-5	202	204	6473	42			6		2				2	
LRC-5	204	206	6474	38			2		ND				2	
LRC-5	206	208	6475	8			5		ND				2	
LRC-5	208	210	6476	13			3		ND	28			2	
LRC-5	210	212	6477	15			4		ND				2	
LRC-5	212	214	6478	37			5		ND				2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-5	214	216	6479	13			4		ND				2	
LRC-5	216	218	6480	40			2		ND				2	
LRC-5	218	220	6481	33			5		ND				2	
LRC-5	220	222	6482	29			2		ND				2	
LRC-5	222	224	6483	16			2		ND				2	
LRC-5	224	226	6484	50			2		ND				2	
LRC-5	226	228	6485	26			5		ND				2	
LRC-5	228	230	6486	46			6		ND	51			2	
LRC-5	230	232	6487	54			4		ND				2	
LRC-5	232	234	6488	16			3		ND				2	
LRC-5	234	236	6489	86			5		5				2	
LRC-5	236	238	6490	68			2		4				2	
LRC-5	238	240	6491	57			4		2				2	
LRC-5	240	242	6492	23			8		ND				2	
LRC-5	242	244	6493	74			4		ND				2	
LRC-5	244	246	6494	6			3		ND				2	
LRC-5	246	248	6495	42			3		ND				2	
LRC-5	248	250	6496	32			2		ND	64			2	
LRC-5	250	252	6497	22			2		ND				2	
LRC-5	252	254	6498	13			3		ND				2	
LRC-5	254	256	6499	51			7		ND				2	
LRC-6	0	2	5870	653			282						2	
LRC-6	2	4	5871	692			320						2	
LRC-6	4	6	5872	760			380						2	
LRC-6	6	8	5873	658			276						2	
LRC-6	8	10	5874	655			310						2	
LRC-6	10	12	5875	772			297						2	
LRC-6	12	14	5876	550			220						2	
LRC-6	14	16	5877	535			250						2	
LRC-6	16	18	5878	869			340						2	
LRC-6	18	20	5879	960			550						2	
LRC-6	20	22	5880	957			269						2	
LRC-6	22	24	5881	650			234						2	
LRC-6	24	26	5882	880			447						2	
LRC-6	26	28	5883	658			280						2	
LRC-6	28	30	5884	574			228						2	
LRC-6	30	32	5885	606			271						2	
LRC-6	32	34	5886	785			330						2	
LRC-6	34	36	5887	806			360						2	
LRC-6	36	38	5888	649			254						2	
LRC-6	38	40	5889	446			184						2	
LRC-6	40	42	5890	494			136						2	
LRC-6	42	44	5891	317			100						2	
LRC-6	44	46	5892	406			146						2	
LRC-6	46	48	5893	516			148						2	
LRC-6	48	50	5894	505			198						2	
LRC-6	50	52	5895	628			270						2	
LRC-6	52	54	5896	720			240						2	
LRC-6	54	56	5897	533			224						2	
LRC-6	56	58	5898	418			168						2	
LRC-6	58	60	5899	308			92						2	
LRC-6	60	62	5900	375			175						2	
LRC-6	62	64	5901	504			218						2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-6	64	66	5902	380			174						2	
LRC-6	66	68	5903	160			50						2	
LRC-6	68	70	5904	790			242						2	
LRC-6	70	72	5905	1047			296						2	
LRC-6	72	74	5906	1288			332						2	
LRC-6	74	76	5907	1107			219						2	
LRC-6	76	78	5908	796			136						2	
LRC-6	78	80	5909	494			132						2	
LRC-6	80	82	5910	540			86						2	
LRC-6	82	84	5911	400			90						2	
LRC-6	84	86	5912	462			61						2	
LRC-6	86	88	5913	542			49						2	
LRC-6	88	90	5914	408			25						2	
LRC-6	90	92	5915	464			97						2	
LRC-6	92	94	5916	1057			271						2	
LRC-6	94	96	5917	590			135						2	
LRC-6	96	98	5918	504			57						2	
LRC-6	98	100	5919	100			55						2	
LRC-7	0	2	5920	158			47						2	
LRC-7	2	4	5921	183			27						2	
LRC-7	4	6	5922	152			21						2	
LRC-7	6	8	5923	244			24						2	
LRC-7	8	10	5924	228			32						2	
LRC-7	10	12	5925	130			13						2	
LRC-7	12	14	5926	154			15						2	
LRC-7	14	16	5927	161			13						2	
LRC-7	16	18	5928	194			13						2	
LRC-7	18	20	5929	199			17						2	
LRC-7	20	22	5930	154			16						2	
LRC-8	0	2	5931	1480			354						2	
LRC-8	2	4	5932	986			180						2	
LRC-8	4	6	5933	1900			520						2	
LRC-8	6	8	5934	1820			463						2	
LRC-8	8	10	5935	1680			332						2	
LRC-8	10	12	5936	1750			350						2	
LRC-8	12	14	5937	1390			303						2	
LRC-8	14	16	5938	1375			280						2	
LRC-8	16	18	5939	1900			482						2	
LRC-8	18	20	5940	1500			492						2	
LRC-8	20	22	5941	1300			480						2	
LRC-8	22	24	5942	1680			658						2	
LRC-8	24	26	5943	1820			934						2	
LRC-8	26	28	5944	1420			596						2	
LRC-8	28	30	5945	1167			305						2	
LRC-8	30	32	5946	1400			520						2	
LRC-8	32	34	5947	1600			860						2	
LRC-8	34	36	5948	1900			1000						2	
LRC-8	36	38	5949	1740			915						2	
LRC-8	38	40	5950	1400			775						2	
LRC-8	40	42	5951	1500			572						2	
LRC-8	42	44	5952	**6850**			3800				6100			2	
LRC-8	44	46	5953	**4800**			2500				4200			2	
LRC-8	46	48	5954	**3700**			1600				3300			2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-8	48	50	5955	3800			2200				3600	0.48%	2	8
LRC-8	50	52	5956	1325			472						2	
LRC-8	52	54	5957	1267			75						2	
LRC-8	54	56	5958	1327			37						2	
LRC-8	56	58	5959	1280			51						2	
LRC-8	58	60	5960	2000			77					0.20%	2	2
LRC-8	60	62	5961	1448			41						2	
LRC-8	62	64	5962	2130			70						2	
LRC-8	64	66	5963	1881			80						2	
LRC-8	66	68	5964	1209			31					0.37%	2	10
LRC-8	68	70	5965	5500			2500				5600		2	
LRC-8	70	72	5966	7700			5600				7900	0.66%	2	4
LRC-8	72	74	5967	763			126						2	
LRC-8	74	76	5968	885			80						2	
LRC-8	76	78	5969	943			75						2	
LRC-8	78	80	5970	1078			57						2	
LRC-8	80	82	5971	778			53						2	
LRC-8	82	84	5972	420			27						2	
LRC-8	84	86	5973	454			29						2	
LRC-8	86	88	5974	484			27						2	
LRC-8	88	90	5975	664			22						2	
LRC-8	90	92	5976	564			32						2	
LRC-8	92	94	5977	482			31						2	
LRC-8	94	96	5978	837			48						2	
LRC-8	96	98	5979	801			36						2	
LRC-8	98	100	5980	674			28						2	
LDD-13	69.8	71	9948	1040									1	
LDD-13	71	72	9949	1380									1	
LDD-13	72	73	9950	1550									1	
LDD-13	73	74	9951	1490									1	
LDD-13	74	75	9952	2310	2300						2464	0.24%	1	
LDD-13	75	76	9953	6740	7100						7280	0.74%	1	
LDD-13	76	77	9954	6210	6200						6360	0.65%	1	
LDD-13	77	78	9955	6630	6900						7260	0.69%	1	
LDD-13	78	79	9956	6970	7400						7480	0.74%	1	
LDD-13	79	80	9957	8370	8900						9340	0.89%	1	
LDD-13	80	81	9958	12400	12700						13000	1.24%	1	
LDD-13	81	82	9959	14720	15100						15000	1.50%	1	
LDD-13	82	83	9960	11820	12400						12000	1.23%	1	
LDD-13	83	84	9961	10490	10650						11000	1.12%	1	
LDD-13	84	85	9962	15000	15000						15000	1.52%	1	
LDD-13	85	86	9963	19100	19100						19000	1.92%	1	
LDD-13	86	87	9964	9230	9500						10000	1.01%	1	
LDD-13	87	88	9965	29240	30000						34000	3.17%	1	
LDD-13	88	89	9966	20340	22000						23000	2.17%	1	
LDD-13	89	90	9967	20960	22300						24000	2.22%	1	
LDD-13	90	91	9968	15540	16000						16000	1.67%	1	
LDD-13	91	92	9969	9520	9700						10000	1.01%	1	
LDD-13	92	93	9970	11660	12200						12000	1.25%	1	
LDD-13	93	94	9971	11620	12300						12000	1.23%	1	
LDD-13	94	95	9972	8450	9900						10000	1.02%	1	
LDD-13	95	96	9973	7990	8400						8660	0.87%	1	
LDD-13	96	97	9974	12040	12600						13000	1.26%	1	

The original results from Plenge Laboratories are used in the composite calculations

Appendix I: Summary of Analyses From Drilling Programs, Lara Project, Peru

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LDD-13	97	98	9975	15740	16350					16000	1.63%		1	
LDD-13	98	99	9976	8780	9100					9280	0.92%		1	
LDD-13	99	100	9977	4370	4500					4740	0.46%		1	
LDD-13	100	101	9978	5650	5800					5860	0.59%		1	
LDD-13	101	102	9979	7800	8200					8240	0.80%		1	
LDD-13	102	103	9980	5580	5900					5900	0.60%	1.15%	1	28
LDD-13	103	104	9981	3223	3200					3540	0.33%		1	
LDD-13	104	105	9982	2970									1	
LDD-13	105	106	9983	3980									1	
LDD-13	106	107	9984	3510									1	
LDD-13	107	108	9985	3010									1	
LDD-13	108	109	9986	2300									1	
LDD-13	109	110	9987	4100									1	
LDD-13	110	110.6	9988	4180								0.95%	1	37
LRC-10	0	2	7030	760			240						2	
LRC-10	2	4	7031	320			80						2	
LRC-10	4	6	7032	175			46						2	
LRC-10	6	8	7033	163			36						2	
LRC-10	8	10	7034	210			54						2	
LRC-10	10	12	7035	149			35						2	
LRC-10	12	14	7036	190			45						2	
LRC-10	14	16	7037	744			176						2	
LRC-10	16	18	7038	205			44						2	
LRC-10	18	20	7039	149			46						2	
LRC-10	20	22	7040	195			47						2	
LRC-10	22	24	7041	124			35						2	
LRC-10	24	26	7042	115			38						2	
LRC-10	26	28	7043	417			115						2	
LRC-10	28	30	7044	160			29						2	
LRC-10	30	32	7045	200			41						2	
LRC-10	32	34	7046	196			40						2	
LRC-10	34	36	7047	200			55						2	
LRC-10	36	38	7048	178			38						2	
LRC-10	38	40	7049	157			40						2	
LRC-10	40	42	7050	186			39						2	
LRC-10	42	44	7051	166			37						2	
LRC-10	44	46	7052	112			36						2	
LRC-10	46	48	7053	200			58						2	
LRC-10	48	50	7054	370			108						2	
LRC-10	50	52	7055	684			306						2	
LRC-10	52	54	7056	1040			559						2	
LRC-10	54	56	7057	1400			786						2	
LRC-10	56	58	7058	600			323						2	
LRC-10	58	60	7059	985			472						2	
LRC-10	60	62	7060	980			520						2	
LRC-10	62	64	7061	3900			1208					0.39%		2	
LRC-10	64	66	7062	5500			1280	3900				0.63%		2	
LRC-10	66	68	7063	5500			1410	3200				0.57%	0.55%	2	4
LRC-10	68	70	7064	4100			1090	2700				0.44%		2	
LRC-10	70	72	7065	6500			1285	3600				0.62%		2	2
LRC-10	72	74	7066	3900			1120	2400				0.42%		2	
LRC-10	74	76	7067	5300			1270	3700				0.60%		2	
LRC-10	76	78	7068	5700			1334	3400				0.59%		2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-10	78	80	7069	8500			1540	4700			0.78%		2	
LRC-10	80	82	7070	5100			1190	3500			0.57%	0.62%	2	8
LRC-10	82	84	7071	4400			875	2700			0.47%		2	
LRC-10	84	86	7072	2700			540	1500			0.29%	0.51%	2	24
LRC-10	86	88	7073	735			100	300			0.09%		2	
LRC-10	88	90	7074	1090			330	700			0.12%		2	
LRC-10	90	92	7075	790			53						2	
LRC-10	92	94	7076	760			34						2	
LRC-10	94	96	7077	700			64						2	
LRC-10	96	98	7078	2400			238						2	
LRC-10	98	100	7079	2300			366						2	
LDD-14	66.9	68	9989	1580									1	
LDD-14	68	69	9990	1280									1	
LDD-14	69	70	9991	5040	4900					4800	0.49%		1	
LDD-14	70	71	9992	2630	2600					2676	0.25%		1	
LDD-14	71	72	9993	1360	1300					1276	0.12%		1	
LDD-14	72	73	9994	10690	10750					11000	1.08%		1	
LDD-14	73	74	9995	7450	7800					7120	0.77%		1	
LDD-14	74	75	9996	14720	15300					15000	1.50%		1	
LDD-14	75	76	9997	11920	12400					12000	1.25%		1	
LDD-14	76	77	9998	10720	10700					10000	1.05%		1	
LDD-14	77	78	9999	8830	9200					9020	0.93%		1	
LDD-14	78	79	10000	19680	21200					22000	2.06%		1	
LDD-14	79	80	10001	11980	13000					13000	1.25%		1	
LDD-14	80	81	10002	12540	12800					13000	1.30%		1	
LDD-14	81	82	10003	10680	11000					11000	1.11%		1	
LDD-14	82	83	10004	8650	8800					9080	0.89%		1	
LDD-14	83	84	10005	7870	8300					8360	0.82%		1	
LDD-14	84	85	10006	8190	8500					8120	0.84%		1	
LDD-14	85	86	10007	15460	16400					15000	1.56%		1	
LDD-14	86	87	10008	8660	9000					8840	0.90%		1	
LDD-14	87	88	10009	10430	10700					10000	1.06%		1	
LDD-14	88	89	10010	15900	16000					16000	1.57%		1	
LDD-14	89	90	10011	7300	7600					7580	0.78%		1	
LDD-14	90	91	10012	41040	41600					42000	4.20%		1	
LDD-14	91	92	10013	11320	11700					12000	1.16%		1	
LDD-14	92	93	10014	12500	12700					13000	1.30%		1	
LDD-14	93	94	10015	8060	8000					8300	0.84%		1	
LDD-14	94	95	10016	8450	8700					8700	0.88%		1	
LDD-14	95	96	10017	6980	7300					7200	0.73%	1.21%	1	24
LDD-14	96	97	10018	3940	4000					4080	0.40%	1.08%	1	28
LDD-14	97	98	10019	1980									1	
LDD-14	98	99	10020	1740									1	
LDD-14	99	100	10021	1880									1	
LDD-14	100	101	10022	5470								0.55%	1	1
LDD-14	101	102	10023	2400									1	
LDD-14	102	103	10024	8790									1	
LDD-14	103	104	10025	6030								0.74%	1	2
LDD-14	104	105	10026	2070									1	
LDD-14	105	106	10027	2070									1	
LDD-14	106	107	10028	1910									1	
LDD-14	107	108	10029	2030								0.38%	1	8
LDD-14	108	108.4	10030	880									1	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-12	0	2	7125	1380			740						2	
LRC-12	2	4	7126	1360			850						2	
LRC-12	4	6	7127	1740			1050						2	
LRC-12	6	8	7128	1050			545						2	
LRC-12	8	10	7129	4750			4100						2	
LRC-12	10	12	7130	2300			1900						2	
LRC-12	12	14	7131	1960			1360						2	
LRC-12	14	16	7132	3400			2070						2	
LRC-12	16	18	7133	3400			1700						2	
LRC-12	18	20	7134	1760			1300						2	
LRC-12	20	22	7135	10200			8700						2	2
LRC-12	22	24	7136	2600			2070						0.38%	2	16
LRC-12	24	26	7137	1580			1100							2	
LRC-12	26	28	7138	1630			1380							2	
LRC-12	28	30	7139	1080			748							2	
LRC-12	30	32	7140	1640			1068							2	
LRC-12	32	34	7141	1610			920							2	
LRC-12	34	36	7142	1740			970							2	
LRC-12	36	38	7143	2160			1038							2	
LRC-12	38	40	7144	2300			1540							2	
LRC-12	40	42	7145	2000			1240							2	
LRC-12	42	44	7146	2600			1370							2	
LRC-12	44	46	7147	5500			2100							2	
LRC-12	46	48	7148	5450			2000						0.55%	2	4
LRC-12	48	50	7149	3700			1400							2	
LRC-12	50	52	7150	2900			947							2	
LRC-12	52	54	7151	7000			1258	3800			0.73%		2	2
LRC-12	54	56	7152	3700			845	2100			0.41%		2	
LRC-12	56	58	7153	3600			918	2100			0.39%		2	
LRC-12	58	60	7154	3570			880	1800			0.38%		2	
LRC-12	60	62	7155	4600			667	1900			0.39%		2	
LRC-12	62	64	7156	3760			635	2200			0.53%		2	
LRC-12	64	66	7157	6500			1028	3000			0.68%		2	
LRC-12	66	68	7158	5800			920	3300			0.65%		2	
LRC-12	68	70	7159	5300			974	2800			0.59%		2	
LRC-12	70	72	7160	6300			1160	3400			0.67%		2	
LRC-12	72	74	7161	5400			1720	3600			0.67%		2	
LRC-12	74	76	7162	6500			3300	4900			0.68%		2	
LRC-12	76	78	7163	7600			3100	5500			0.82%		2	
LRC-12	78	80	7164	6300			1815	3900			0.66%		2	
LRC-12	80	82	7165	7300			1670	4000			0.77%		2	
LRC-12	82	84	7166	10200			2900	8200			1.17%		2	
LRC-12	84	86	7167	9700			2500	6700			1.02%		2	
LRC-12	86	88	7168	12000			2500	8500			1.30%		2	
LRC-12	88	90	7169	6600			2070	4000			0.70%	0.73%	2	26
LRC-12	90	92	7170	3300			450	1100			0.35%		2	
LRC-12	92	94	7171	2400			410	900			0.26%		2	
LRC-12	94	96	7172	4600			550	1100			0.50%		2	
LRC-12	96	98	7173	3000			316	900			0.30%		2	
LRC-12	98	100	7174	2070			202	600			0.24%	0.51%	2	64
LRC-15	0	2	9521	135										
LRC-15	2	4	9522	162										
LRC-15	4	6	9523	180										

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-15	6	8	9524	200										
LRC-15	8	10	9525	210										
LRC-15	10	12	9526	139										
LRC-15	12	14	9527	116										
LRC-15	14	16	9528	177										
LRC-15	16	18	9529	170										
LRC-15	18	20	9530	167										
LRC-15	20	22	9531	205										
LRC-15	22	24	9532	266										
LRC-15	24	26	9533	315										
LRC-15	26	28	9534	252										
LRC-15	28	30	9535	282										
LRC-15	30	32	9536	252										
LRC-15	32	34	9537	281										
LRC-15	34	36	9538	264										
LRC-15	36	38	9539	219										
LRC-15	38	40	9540	234										
LRC-15	40	42	9541	271										
LRC-15	42	44	9542	415										
LRC-15	44	46	9543	580										
LRC-15	46	48	9544	826										
LRC-15	48	50	9545	1380										
LRC-15	50	52	9546	1700										
LRC-15	52	54	9547	1190										
LRC-15	54	56	9548	783										
LRC-15	56	58	9549	1132										
LRC-15	58	60	9550	6000						6340	0.66%		2	
LRC-15	60	62	9551	12900						13000	1.31%		2	
LRC-15	62	64	9552	13000						12000	1.38%		2	
LRC-15	64	66	9553	10600						10000	1.09%		2	
LRC-15	66	68	9554	12900						13000	1.18%		2	
LRC-15	68	70	9555	11900						12000	1.25%		2	
LRC-15	70	72	9556	10700						10000	1.08%		2	
LRC-15	72	74	9557	11500						12000	1.28%	1.12%	2	16
LRC-15	74	76	9558	2850						3060	0.30%		2	
LRC-15	76	78	9559	2900						3040	0.31%		2	
LRC-15	78	80	9560	4350						4500	0.45%		2	
LRC-15	80	82	9561	2370									2	
LRC-15	82	84	9562	2320									2	
LRC-15	84	86	9563	2380									2	
LRC-15	86	88	9564	2530									2	
LRC-15	88	90	9565	5610								0.56%	2	2
LRC-15	90	92	9566	2370									2	
LRC-15	92	94	9567	3770									2	
LRC-15	94	96	9568	3000									2	
LRC-15	96	98	9569	2850									2	
LRC-15	98	100	9570	3670									2	
LRC-15	100	102	9571	4080								0.61%	2	44
LRC-16	0	2	9572	550										
LRC-16	2	4	9573	540										
LRC-16	4	6	9574	598										
LRC-16	6	8	9575	1320										
LRC-16	8	10	9576	640										

The original results from Plenge Laboratories are used in the composite calculations

Appendix I: Summary of Analyses From Drilling Programs, Lara Project, Peru

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-16	10	12	9577	731										
LRC-16	12	14	9578	668										
LRC-16	14	16	9579	566										
LRC-16	16	18	9580	503										
LRC-16	18	20	9581	520										
LRC-16	20	22	9582	503										
LRC-16	22	24	9583	535										
LRC-16	24	26	9584	540										
LRC-16	26	28	9585	900										
LRC-16	28	30	9586	940										
LRC-16	30	32	9587	1262										
LRC-16	32	34	9588	603										
LRC-16	34	36	9589	286										
LRC-16	36	38	9590	3230							3320	0.33%		2	
LRC-16	38	40	9591	4310							4520	0.42%		2	
LRC-16	40	42	9592	4465							4440	0.43%		2	
LRC-16	42	44	9593	5520							5500	0.57%	0.55%	2	2
LRC-16	44	46	9594	4800							4900	0.46%	0.45%	2	10
LRC-16	46	48	9595	1496											
LRC-16	48	50	9596	1100											
LRC-16	50	52	9597	1008											
LRC-16	52	54	9598	900											
LRC-16	54	56	9599	164											
LRC-16	56	58	9600	151											
LRC-16	58	60	9601	373											
LRC-16	60	62	9602	363											
LRC-16	62	64	9603	1632											
LRC-16	64	66	9604	2035									0.20%	2	2
LRC-16	66	68	9605	374											
LRC-16	68	70	9606	358											
LRC-16	70	72	9607	193											
LRC-16	72	74	9608	186											
LRC-16	74	76	9609	258											
LRC-16	76	78	9610	1282											
LRC-16	78	80	9611	405											
LRC-16	80	82	9612	1790											
LRC-16	82	84	9613	2650										2	
LRC-16	84	86	9614	2710										2	
LRC-16	86	88	9615	1855										2	
LRC-16	88	90	9616	4209									0.29%	2	8
LRC-16	90	92	9617	1306											
LRC-16	92	94	9618	874											
LRC-16	94	96	9619	1025											
LRC-16	96	98	9620	1665											
LRC-16	98	100	9621	1605											
LRC-18	0	2	9622	416											
LRC-18	2	4	9623	317											
LRC-18	4	6	9624	177											
LRC-18	6	8	9625	214											
LRC-18	8	10	9626	157											
LRC-18	10	12	9627	212											
LRC-18	12	14	9628	254											
LRC-18	14	16	9629	200											

The original results from Plenge Laboratories are used in the composite calculations

Appendix I: Summary of Analyses From Drilling Programs, Lara Project, Peru

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-18	16	18	9630	240										
LRC-18	18	20	9631	244										
LRC-18	20	22	9632	250										
LRC-18	22	24	9633	246										
LRC-18	24	26	9634	200										
LRC-18	26	28	9635	275										
LRC-18	28	30	9636	255										
LRC-18	30	32	9637	370										
LRC-18	32	34	9638	472										
LRC-18	34	36	9639	411										
LRC-18	36	38	9640	516										
LRC-18	38	40	9641	901										
LRC-18	40	42	9642	594										
LRC-18	42	44	9643	584										
LRC-18	44	46	9644	720										
LRC-18	46	48	9645	970										
LRC-18	48	50	9646	975										
LRC-18	50	52	9647	939										
LRC-18	52	54	9648	732										
LRC-18	54	56	9649	928										
LRC-18	56	58	9650	1000										
LRC-18	58	60	9651	1440										
LRC-18	60	62	9652	1300										
LRC-18	62	64	9653	1080										
LRC-18	64	66	9654	1280										
LRC-18	66	68	9655	1395										
LRC-18	68	70	9656	775										
LRC-18	70	72	9657	870										
LRC-18	72	74	9658	790										
LRC-18	74	76	9659	816										
LRC-18	76	78	9660	629										
LRC-18	78	80	9661	583										
LRC-18	80	82	9662	940										
LRC-18	82	84	9663	830										
LRC-18	84	86	9664	960										
LRC-18	86	88	9665	1400										
LRC-18	88	90	9666	1200										
LRC-19	0	2	9667	340										
LRC-19	2	4	9668	238										
LRC-19	4	6	9669	343										
LRC-19	6	8	9670	xxx										
LRC-19	8	10	9671	245										
LRC-19	10	12	9672	332										
LRC-19	12	14	9673	305										
LRC-19	14	16	9674	270										
LRC-19	16	18	9675	316										
LRC-19	18	20	9676	369										
LRC-19	20	22	9677	530										
LRC-19	22	24	9678	409										
LRC-19	24	26	9679	331										
LRC-19	26	28	9680	373										
LRC-19	28	30	9681	423										
LRC-19	30	32	9682	2200						2540	0.24%	0.22%	2	2

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-19	32	34	9683	1800						1972	0.20%			
LRC-19	34	36	9684	1700						1822	0.18%			
LRC-19	36	38	9685	2400						2460	0.24%		2	
LRC-19	38	40	9686	2390						2460	0.27%		2	
LRC-19	40	42	9687	5700						5560	0.58%		2	
LRC-19	42	44	9688	9150						6100	0.96%		2	
LRC-19	44	46	9689	14400						15000	1.53%		2	4
LRC-19	46	48	9690	5000						5460	0.60%	0.86%	2	
LRC-19	48	50	9691	4900						5160	0.55%		2	
LRC-19	50	52	9692	3370						3720	0.35%	0.59%	2	16
LRC-19	52	54	9693	1415										
LRC-19	54	56	9694	1438										
LRC-19	56	58	9695	1586										
LRC-19	58	60	9696	790										
LRC-19	60	62	9697	2170										
LRC-19	62	64	9698	1340										
LRC-19	64	66	9699	1670										
LRC-19	66	68	9700	1725										
LRC-19	68	70	9701	950										
LRC-19	70	72	9702	1347										
LRC-19	72	74	9703	1400										
LRC-19	74	76	9704	2490										
LRC-19	76	78	9705	1210										
LRC-19	78	80	9706	1317										
LRC-19	80	82	9707	1610										
LRC-19	82	84	9708	1048										
LRC-19	84	86	9709	1233										
LRC-19	86	88	9710	1565										
LRC-19	88	90	9711	1572										
LRC-19	90	92	9712	4605										
LRC-19	92	94	9713	1540										
LRC-19	94	96	9714	984										
LRC-20	0	2	9715	187										
LRC-20	2	4	9716	190										
LRC-20	4	6	9717	124										
LRC-20	6	8	9718	170										
LRC-20	8	10	9719	171										
LRC-20	10	12	9720	168										
LRC-20	12	14	9721	265										
LRC-20	14	16	9722	340										
LRC-20	16	18	9723	405										
LRC-20	18	20	9724	640										
LRC-20	20	22	9725	1664										
LRC-20	22	24	9726	3090						3240	0.31%		2	
LRC-20	24	26	9727	3750						3760	0.37%		2	
LRC-20	26	28	9728	3390						3540	0.34%		2	
LRC-20	28	30	9729	3440						3660	0.36%		2	
LRC-20	30	32	9730	3520						3540	0.33%		2	
LRC-20	32	34	9731	3430						3440	0.33%		2	
LRC-20	34	36	9732	4650						5120	0.49%		2	
LRC-20	36	38	9733	2480						2860	0.27%	0.35%	2	16
LRC-20	38	40	9734	1715										
LRC-20	40	42	9735	1990										

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-20	42	44	9736	1997										
LRC-20	44	46	9737	1604										
LRC-20	46	48	9738	1336										
LRC-20	48	50	9739	2520										
LRC-20	50	52	9740	4630										
LRC-20	52	54	9741	2085										
LRC-20	54	56	9742	913										
LRC-20	56	58	9743	836										
LRC-20	58	60	9744	1060										
LRC-20	60	62	9745	2060										
LRC-20	62	64	9746	1123										
LRC-20	64	66	9747	2016										
LRC-20	66	68	9748	3630										
LRC-20	68	70	9749	1430										
LRC-20	70	72	9750	1493										
LRC-20	72	74	9751	1100										
LRC-20	74	76	9752	1574										
LRC-20	76	78	9753	1500										
LRC-20	78	80	9754	2970										
LRC-20	80	82	9755	1050										
LRC-20	82	84	9756	1595										
LRC-20	84	86	9757	1317										
LRC-20	86	88	9758	1216										
LRC-20	88	90	9759	1941										
LRC-20	90	92	9760	2143										
LRC-20	92	94	9761	2065										
LRC-20	94	96	9762	3310										
LRC-21	0	2	9763	269										
LRC-21	2	4	9764	245										
LRC-21	4	6	9765	207										
LRC-21	6	8	9766	163										
LRC-21	8	10	9767	160										
LRC-21	10	12	9768	131										
LRC-21	12	14	9769	1054										
LRC-21	14	16	9770	278										
LRC-21	16	18	9771	392										
LRC-21	18	20	9772	230										
LRC-21	20	22	9773	189										
LRC-21	22	24	9774	246										
LRC-21	24	26	9775	381										
LRC-21	26	28	9776	818										
LRC-21	28	30	9777	395										
LRC-21	30	32	9778	488										
LRC-21	32	34	9779	478										
LRC-21	34	36	9780	680										
LRC-21	36	38	9781	2970									2	
LRC-21	38	40	9782	4400								0.37%	2	4
LRC-21	40	42	9783	1384										
LRC-21	42	44	9784	1455										
LRC-21	44	46	9785	1213										
LRC-21	46	48	9786	1400										
LRC-21	48	50	9787	1971										
LRC-21	50	52	9788	1627										

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-21	52	54	9789	1790										
LRC-21	54	56	9790	1496										
LRC-21	56	58	9791	1623										
LRC-21	58	60	9792	3480									2	
LRC-21	60	62	9793	3100								0.33%	2	4
LRC-21	62	64	9794	1168										
LRC-21	64	66	9795	1186										
LRC-21	66	68	9796	1435										
LRC-21	68	70	9797	1820										
LRC-21	70	72	9798	1881										
LRC-21	72	74	9799	1640										
LRC-21	74	76	9800	1300										
LRC-21	76	78	9801	1547										
LRC-21	78	80	9802	5830						6240	0.66%		2	
LRC-21	80	82	9803	11270						11000	1.21%		2	
LRC-21	82	84	9804	16900						18000	1.85%		2	
LRC-21	84	86	9805	14100						15000	1.61%		2	
LRC-21	86	88	9806	13900						15000	1.51%		2	
LRC-21	88	90	9807	13200						14000	1.42%		2	
LRC-21	90	92	9808	10900						12000	1.22%	1.23%	2	14
LRC-21	92	94	9809	4840						5560	0.55%		2	
LRC-21	94	96	9810	3390						3800	0.37%		2	
LRC-21	96	98	9811	3000						3180	0.31%		2	
LRC-21	98	100	9812	3180						3220	0.31%		2	
LRC-21	100	102	9813	3650						3520	0.34%		2	
LRC-21	102	104	9814	4570						4760	0.46%		2	
LRC-21	104	106	9815	5300						5500	0.57%	0.53%	2	2
LRC-21	106	108	9816	3770						3980	0.39%		2	
LRC-21	108	110	9817	7620						8140	0.84%	0.76%	2	2
LRC-21	110	112	9818	3310						3760	0.35%		2	
LRC-21	112	114	9819	4485						4640	0.44%	0.74%	2	36
LRC-22	0	2	9820	208										
LRC-22	2	4	9821	1803										
LRC-22	4	6	9822	414										
LRC-22	6	8	9823	recuperación de muestra										
LRC-22	8	10	9824	434										
LRC-22	10	12	9825	572										
LRC-22	12	14	9826	452										
LRC-22	14	16	9827	412										
LRC-22	16	18	9828	394										
LRC-22	18	20	9829	318										
LRC-22	20	22	9830	280										
LRC-22	22	24	9831	297										
LRC-22	24	26	9832	326										
LRC-22	26	28	9833	339										
LRC-22	28	30	9834	560										
LRC-22	30	32	9835	383										
LRC-22	32	34	9836	310										
LRC-22	34	36	9837	266										
LRC-22	36	38	9838	423										
LRC-22	38	40	9839	372										
LRC-22	40	42	9840	319										
LRC-22	42	44	9841	436										

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-22	44	46	9842	502										
LRC-22	46	48	9843	846										
LRC-22	48	50	9844	692										
LRC-22	50	52	9845	625										
LRC-22	52	54	9846	860										
LRC-22	54	56	9847	846										
LRC-22	56	58	9848	788										
LRC-22	58	60	9849	810										
LRC-22	60	62	9850	1000										
LRC-22	62	64	9851	1108										
LRC-22	64	66	9852	883										
LRC-22	66	68	9853	707										
LRC-22	68	70	9854	754										
LRC-22	70	72	9855	1058										
LRC-22	72	74	9856	1138										
LRC-22	74	76	9857	1074										
LRC-22	76	78	9858	1014										
LRC-22	78	80	9859	1834										
LRC-22	80	82	9860	1147										
LRC-22	82	84	9861	1223										
LRC-22	84	86	9862	3750							4020	0.38%		2	
LRC-22	86	88	9863	6900							7240	0.68%		2	
LRC-22	88	90	9864	13300							14000	1.41%		2	
LRC-22	90	92	9865	6300							6480	0.67%		2	
LRC-22	92	94	9866	4800							5080	0.49%		2	
LRC-22	94	96	9867	14000							14000	1.48%		2	
LRC-22	96	98	9868	10200							9540	1.01%		2	
LRC-22	98	100	9869	10900							11000	1.09%		2	
LRC-22	100	102	9870	12800							13000	1.33%		2	
LRC-22	102	104	9871	5900							6460	0.62%		2	
LRC-22	104	106	9872	5450							5100	0.46%		2	
LRC-22	106	108	9873	7800							7720	0.78%		2	
LRC-22	108	110	9874	6600							6860	0.69%	0.84%	2	26
LRC-22	110	112	9875	2590										2	
LRC-22	112	114	9876	2910										2	
LRC-22	114	116	9877	2400										2	
LRC-22	116	118	9878	2720										2	
LRC-22	118	120	9879	2840									0.68%	2	36
LRC-23	0	2	9880	1763										2	
LRC-23	2	4	9881	1121										2	
LRC-23	4	6	9882	1204										2	
LRC-23	6	8	9883	819										2	
LRC-23	8	10	9884	575										2	
LRC-23	10	12	9885	1390										2	
LRC-23	12	14	9886	1312										2	
LRC-23	14	16	9887	1280										2	
LRC-23	16	18	9888	1370										2	
LRC-23	18	20	9889	1485										2	
LRC-23	20	22	9890	1580										2	
LRC-23	22	24	9891	1490										2	
LRC-23	24	26	9892	1900										2	
LRC-23	26	28	9893	2360							2500	0.26%		2	
LRC-23	28	30	9894	2840							2920	0.30%		2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-23	30	32	9895	3800						4160	0.40%		2	
LRC-23	32	34	9896	3100						3400	0.34%		2	
LRC-23	34	36	9897	3000						3040	0.29%		2	
LRC-23	36	38	9898	3730						4500	0.42%		2	
LRC-23	38	40	9899	3160						3620	0.34%		2	
LRC-23	40	42	9900	3750						4360	0.42%		2	
LRC-23	42	44	9901	4940						5340	0.54%		2	
LRC-23	44	46	9902	4080						4280	0.44%		2	
LRC-23	46	48	9903	3550						3780	0.40%		2	
LRC-23	48	50	9904	3400						3720	0.37%		2	
LRC-23	50	52	9905	4200						4320	0.43%		2	
LRC-23	52	54	9906	2800						3060	0.31%		2	
LRC-23	54	56	9907	5650						5640	0.60%	0.57%	2	2
LRC-23	56	58	9908	4300						4440	0.45%		2	
LRC-23	58	60	9909	5080						5220	0.54%	0.51%	2	2
LRC-23	60	62	9910	4750						4768	0.46%		2	
LRC-23	62	64	9911	4080						4228	0.41%		2	
LRC-23	64	66	9912	5870						5920	0.63%	0.59%	2	2
LRC-23	66	68	9913	4910						5040	0.54%		2	
LRC-23	68	70	9914	3900						3900	0.39%		2	
LRC-23	70	72	9915	3240						3180	0.33%		2	
LRC-23	72	74	9916	4470						4620	0.47%		2	
LRC-23	74	76	9917	4000						4240	0.42%		2	
LRC-23	76	78	9918	4580						4880	0.48%		2	
LRC-23	78	80	9919	2900						3260	0.32%		2	
LRC-23	80	82	9920	3450						3780	0.37%		2	
LRC-23	82	84	9921	3580						4020	0.38%		2	
LRC-23	84	86	9922	3000						3400	0.34%		2	
LRC-23	86	88	9923	2300						2420	0.25%		2	
LRC-23	88	90	9924	2400	4025					2320	0.24%	0.38%	2	64
LRC-24	0	2	9925	495									2	
LRC-24	2	4	9926	590									2	
LRC-24	4	6	9927	666									2	
LRC-24	6	8	9928	541									2	
LRC-24	8	10	9929	671									2	
LRC-24	10	12	9930	696									2	
LRC-24	12	14	9931	690									2	
LRC-24	14	16	9932	883									2	
LRC-24	16	18	9933	1000									2	
LRC-24	18	20	9934	1366									2	
LRC-24	20	22	9935	2100								0.21%	2	2
LRC-24	22	24	9936	1690									2	
LRC-24	24	26	9937	1695									2	
LRC-24	26	28	9938	1750									2	
LRC-24	28	30	9939	1843									2	
LRC-24	30	32	9940	2300								0.23%	2	2
LRC-24	32	34	9941	1574									2	
LRC-24	34	36	9942	1375									2	
LRC-24	36	38	9943	2250									2	
LRC-24	38	40	9944	2970									2	
LRC-24	40	42	9945	1894									2	
LRC-24	42	44	9946	2700									2	
LRC-24	44	46	9947	2480									1.2	

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-24	45.2	46	10038	2570								0.25%	0.8	10
LRC-24	46	47	10039	1600									1	
LRC-24	47	48	10040	1530									1	
LRC-24	48	49	10041	1450									1	
LRC-24	49	50	10042	2090								0.21%	1	2
LRC-24	50	51	10043	1250									1	
LRC-24	51	52	10044	1390									1	
LRC-24	52	53	10045	1470									1	
LRC-24	53	54	10046	1490									1	
LRC-24	54	55	10047	1270									1	
LRC-24	55	56	10048	1280									1	
LRC-24	56	57	10049	1770									1	
LRC-24	57	58	10050	1380									1	
LRC-24	58	59	10051	1550									1	
LRC-24	59	60	10052	2750									1	
LRC-24	60	61	10053	4720									1	
LRC-24	61	62	10054	2110								0.32%	1	3
LRC-24	62	63	10055	1390									1	
LRC-24	63	64	10056	1790									1	
LRC-24	64	65	10057	2950									1	
LRC-24	65	66	10058	5890									1	
LRC-24	66	67	10059	5090								0.55%	1	2
LRC-24	67	68	10060	3620									1	
LRC-24	68	69	10061	2120								0.39%	1	5
LRC-24	69	70	10062	1330									1	
LRC-24	70	71	10063	1720									1	
LRC-24	71	72	10064	2140								0.21%	1	1
LRC-24	72	73	10065	880									1	
LRC-24	73	74	10066	3570	3600					3580	0.34%		1	
LRC-24	74	75	10067	2580	2500					2540	0.25%		1	
LRC-24	75	76	10068	1720	1600					1662	0.16%		1	
LRC-24	76	77	10069	2280	2200					2350	0.21%		1	
LRC-24	77	78	10070	2860	2800					2880	0.28%		1	
LRC-24	78	79	10071	4560	4700					4800	0.45%		1	
LRC-24	79	80	10072	3700	3700					3620	0.34%		1	
LRC-24	80	81	10073	3660	3800					3670	0.36%		1	
LRC-24	81	82	10074	5440	5300					5430	0.54%		1	
LRC-24	82	83	10075	5360	5400					5560	0.53%		1	
LRC-24	83	84	10076	6110	6200					6390	0.63%		1	
LRC-24	84	85	10077	5940	6100					5980	0.59%	0.59%	1	5
LRC-24	85	86	10078	6650	6450	4092.30769				6540	0.64%	0.42%	1	13
LRC-24	86	87	10079	1300									1	
LRC-24	87	88	10080	1780									1	
LRC-24	88	89	10081	2120									1	
LRC-24	89	89.7	10082	2560								0.23%	0.7	1.7
LRC-9A	0	2	5981	190										
LRC-9A	2	4	5982	300										
LRC-9A	4	6	5983	1050										
LRC-9A	6	8	5984	2920									2	
LRC-9A	8	10	5985	2650								0.28%	2	4
LRC-9A	10	12	5986	744										
LRC-9A	12	14	5987	313										
LRC-9A	14	16	5988	3300								0.33%	2	2

The original results from Plenge Laboratories are used in the composite calculations

Appendix I: Summary of Analyses From Drilling Programs, Lara Project, Peru

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-9A	16	18	5989	290										
LRC-9A	18	20	5990	220										
LRC-9A	20	22	5991	220										
LRC-9A	22	24	5992	129										
LRC-9A	24	26	5993	772										
LRC-9A	26	28	5994	475										
LRC-9A	28	30	5995	570										
LRC-9A	30	32	5996	279										
LRC-9A	32	34	5997	364										
LRC-9A	34	36	5998	324										
LRC-9A	36	38	5999	410										
LRC-9A	38	40	6000	523										
LRC-9A	40	42	7001	358										
LRC-9A	42	44	7002	420										
LRC-9A	44	46	7003	442										
LRC-9A	46	48	7004	868										
LRC-9A	48	50	7005	1120										
LRC-9A	50	52	7006	916										
LRC-9A	52	54	7007	1100										
LRC-9A	54	56	7008	1050										
LRC-9A	56	58	7009	1175										
LRC-9A	58	60	7010	1530										
LRC-9A	60	62	7011	1900										
LRC-9A	62	64	7012	1960										
LRC-9A	64	66	7013	1600										
LRC-9A	66	68	7014	1010										
LRC-9A	68	70	7015	900										
LRC-9A	70	72	7016	1000										
LRC-9A	72	74	7017	1000										
LRC-9A	74	76	7018	5600								0.49%			
LRC-9A	76	78	7019	10200								1.00%			
LRC-9A	78	80	7020	11000								1.08%			
LRC-9A	80	82	7021	11500								1.14%			
LRC-9A	82	84	7022	10800								1.07%			
LRC-9A	84	86	7023	8400								0.74%			
LRC-9A	86	88	7024	12700								1.23%			
LRC-9A	88	90	7025	10700								1.10%			
LRC-9A	90	92	7026	11600								1.15%			
LRC-9A	92	94	7027	9350								0.90%			
LRC-9A	94	96	7028	12850								1.31%			
LRC-9A	96	98	7029	19300								1.93%			
LRC-11	0	2	7080	480										
LRC-11	2	4	no sample											
LRC-11	4	6	7081	690										
LRC-11	6	8	7082	460										
LRC-11	8	10	7083	500										
LRC-11	10	12	7084	660										
LRC-11	12	14	7085	480										
LRC-11	14	16	7086	590										
LRC-11	16	18	7087	820										
LRC-11	18	20	7088	715										
LRC-11	20	22	7089	920										
LRC-11	22	24	7090	905										

Appendix I: Summary of Analyses From Drilling Programs, Lara Project, Peru

The original results from Plenge Laboratories are used in the composite calculations

Hole	From (metres)	To (metres)	Sample	PPM Cu (orig.) (Plenge)	PPM Cu (check) (Plenge)	% Total Cu (Plenge)	PPM Cu (sol) (Plenge)	Cu(Sol) (IPL)	PPM Mo (Plenge)	PPM Cu (IPL)	%Total Cu (IPL)	Weighted Avg.	Sample Intv	Cum. interval
LRC-11	24	26	7091	1000										
LRC-11	26	28	7092	630										
LRC-11	28	30	7093	618										
LRC-11	30	32	7094	590										
LRC-11	32	34	7095	1540										
LRC-11	34	36	7096	1550										
LRC-11	36	38	7097	1600										
LRC-11	38	40	7098	1440										
LRC-11	40	42	7099	1260										
LRC-11	42	44	7100	1070										
LRC-11	44	46	7101	1030										
LRC-11	46	48	7102	1160										
LRC-11	48	50	7103	1380										
LRC-11	50	52	7104	1900										
LRC-11	52	54	7105	**3000**									2	
LRC-11	54	56	7106	**3300**									2	
LRC-11	56	58	7107	**2400**								**0.29%**	2	**6**
LRC-11	58	60	7108	1140										
LRC-11	60	62	7109	1190										
LRC-11	62	64	7110	1480										
LRC-11	64	66	7111	1280										
LRC-11	66	68	7112	1190										
LRC-11	68	70	7113	1935										
LRC-11	70	72	7114	2100							0.22%			
LRC-11	72	74	7115	2400							0.23%			
LRC-11	74	76	7116	4300							0.39%			
LRC-11	76	78	7117	2170							0.23%			
LRC-11	78	80	7118	3600							0.38%			
LRC-11	80	82	7119	12800	4900			11800			1.32%			
LRC-11	82	84	7120	16000	8700			17000			1.76%			
LRC-11	84	86	7121	12100	7300			12300			1.26%			
LRC-11	86	88	7122	2300	400			900			0.28%			
LRC-11	88	90	7123	11800	4300			9700			1.27%			
LRC-11	90	92	7124	6300	1500			3300			0.71%			

The original results from Plenge Laboratories are used in the composite calculations

Appendix II

Proposed Budget

and

Drill Hole Summary

PROPOSED HOLE	INCLINATION (degrees)	R.C. HOLE (metres)	DDH (metres)	TOTAL (metres)
A	-90	50	50	100
B	-90	50	50	100
C	-90	50	50	100
D	-90	50	50	100
E	-90	50	50	100
F	-90	50	50	100
G	-90	50	50	100
H	-90	50	50	100
I	-90	50	50	100
J	-90	100	50	150
K	-90	100	50	150
L	-90	100	50	150
M	-90	60	50	110
N	-90	60	50	110
O	-90	60	50	110
P	-90	60	50	110
Q	-90	60	50	110
R	-90	100	50	150
S	-90	100	50	150
T	-90	100	50	150
U	-90	100	50	150
V	-90	100	50	150
W	-90	100	50	150
X	-90	40	60	100
Y	-90	40	60	100
TOTALS:		1730	1270	3000

Appendix II. Proposed Budget and Drill Hole Summary

DESCRIPTION	RATE	UNITS	COST
	US$	hours, m, etc.	US$
Road/Site Construction (all inclusive)	$125	200	$25,000
Drilling Costs (all inclusive)	$110	3000	$330,000
Project Manager - Qualified Person/Professional Geologist	$400	60	$24,000
Geological Staff			$35,000
Salaries: personnel and assistants, labourers			
Analyses	$15	500	$7,500
500 core samples (2 metre spacing) @$15.00/sample			
Camp Expenses	$80	60	$4,800
Food, accommodations (6 people)			
Miscellaneous	$100	60	$6,000
core boxes. truck rentals, fuel			
International Travel			$4,000
TOTAL:			**$436,300**
Canadian funds @ C$1.20 per US$1.00			$523,560
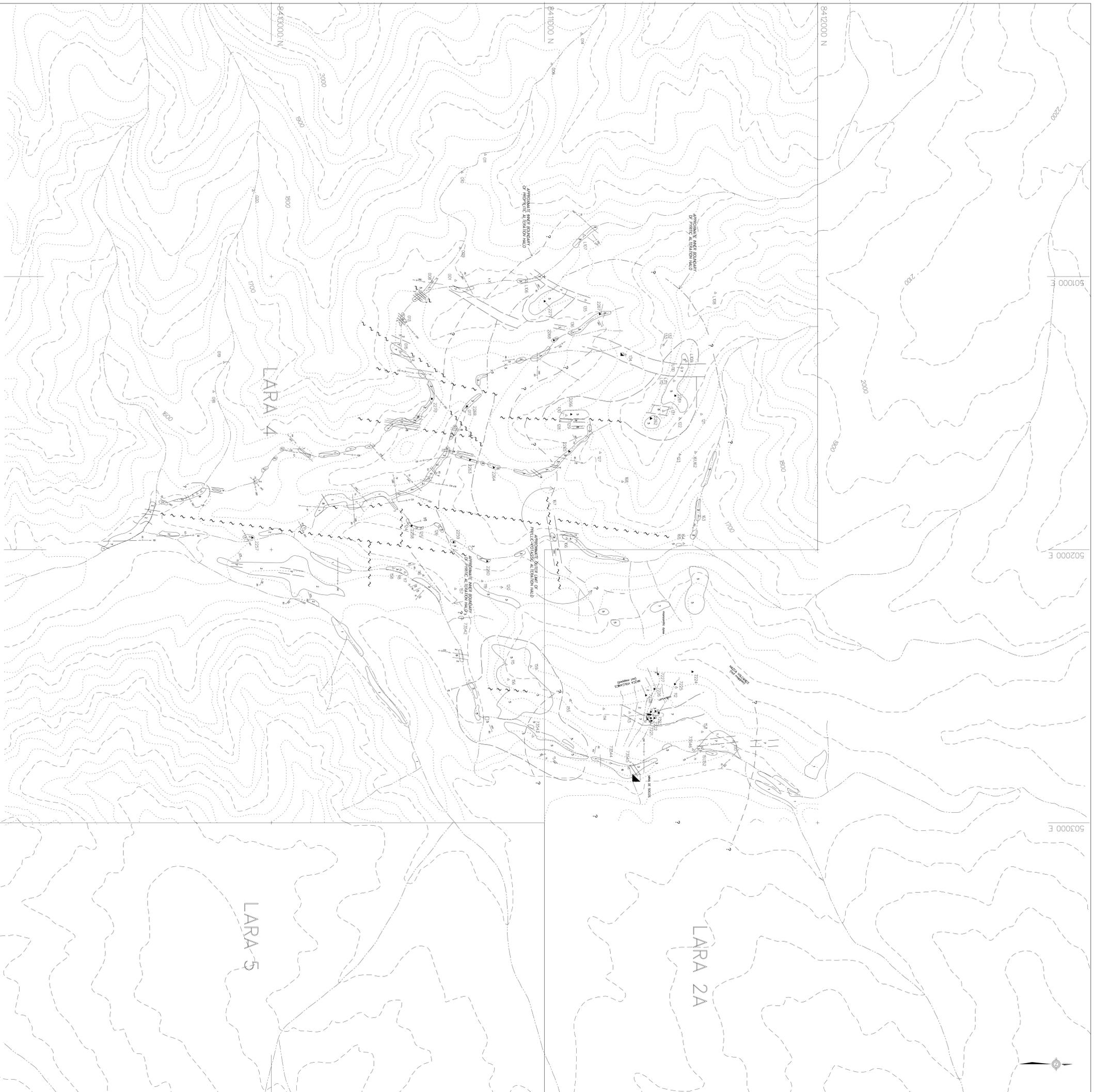
LARA 4

LARA 5

LARA 2A

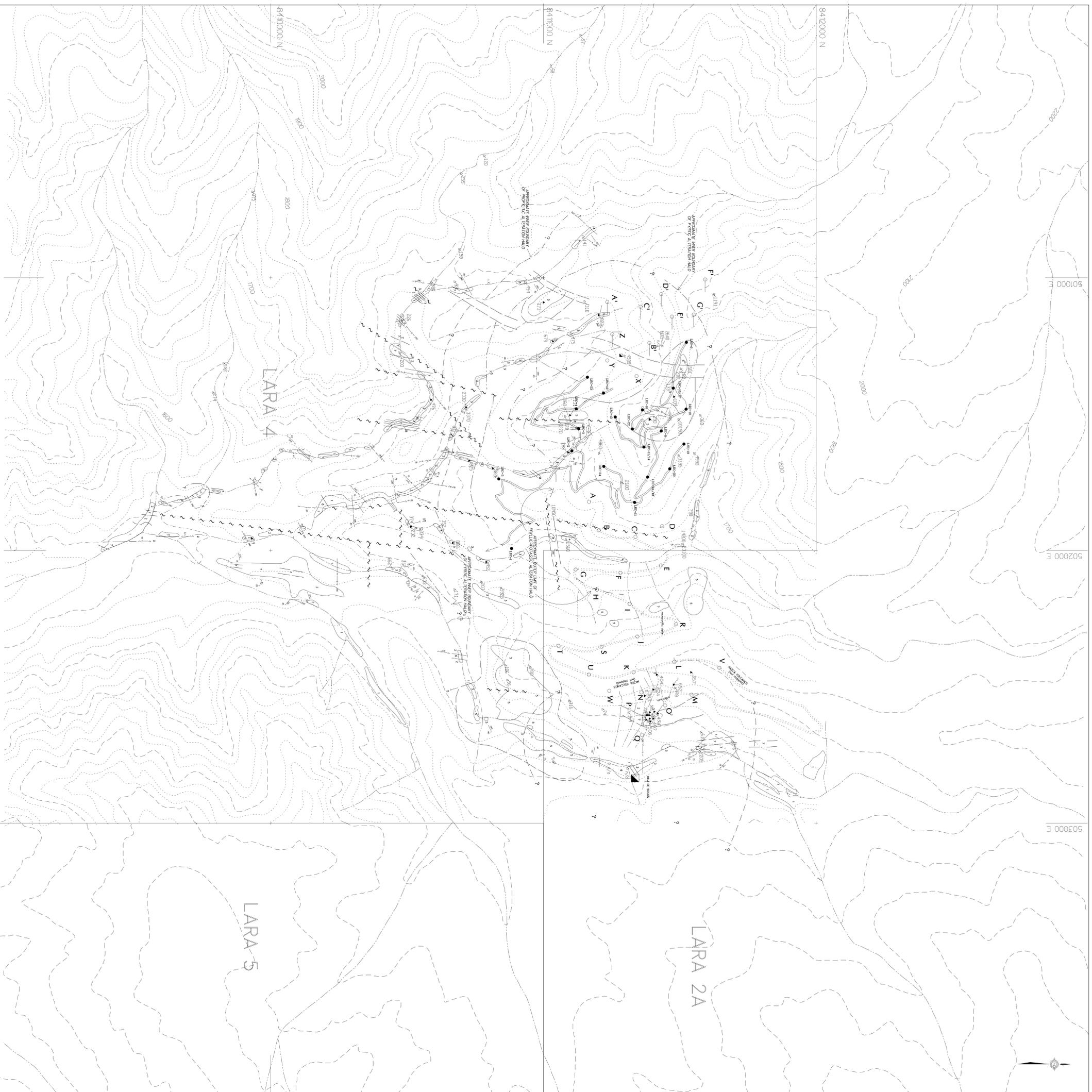8412000 N

8411000 N

8410000 N

501000 E

502000 E

503000 E

LEGEND

9 BRECCIA PIPE: Post-andesite porphyry

8 DACITE DYKES: Light coloured, beige to green; contains copper carbonates +/- tenorite/neotocite within porphyry 'halo'

7 PORPHYRITIC ANDESITE DYKES: Plagioclase-hornblende +/- biotite phenocrysts

6 DACITE PORPHYRY: Dark grey to black, fresh, contains disseminated and fracture filled pyrite and chalcopyrite; possibly a volcanic neck

5 QUARTZ MONZONITE/GRANITE/APLITE PORPHYRY: Hematized and veined with quartz—locally as stockworks

4 SERICITIC APLITE/QUARTZ MONZONITE PHASE: Contains diorite-monzonite phase locally. Secondary biotite is common; contains minor copper carbonate +/- tenorite/neotocite

3 ARGILLIC ALTERED PORPHYRY (DIORITE): Includes argillic, phyllic and pyritic halo phases (see map). Variously veined with limonites, hematite, quartz and gypsum

2 PROPYLITIZED DIORITE: Epidote, chlorite, calcite. Includes pyritic halo locally

1 UNALTERED DIORITE: Includes some monzonite, but dominantly dioritic in composition

⌇⌇⌇ Major fault

—— Geologic contact

⟋ Fault slip

⟋ Fault orientation: inclined, vertical

⟋ Joint orientation: inclined, vertical

◯ Area of outcrop

2206 Rock samples collected by J. Nebocat (July, 1995, May, 1997); R. Tejada (Aug, 1999.)

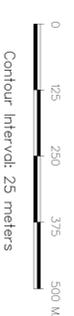Rock Samples collected by Carlos E. Villafuerte (1994, 1995)

LARA EXPLORATION LTD.

LARA 2A & 4 CLAIMS
PROPERTY GEOLOGY

SCALE	DATE (REV.)	DRAWN BY	FIGURE
1:5000	FEB. 9, 2004	JN	MAP 1

Contour interval: 25 meters

0   125   250   375   500 M

Contour interval: 25 meters

LARA 4

LARA 5

LARA 2A

8412000 N

8411000 N

8410000 N

LEGEND

9 BRECCIA PIPE: Post—andesite porphyry

8 DACITE DYKES: Light coloured, beige to green, contains copper carbonates +/− tenorite/neotocite within porphyry 'halo'

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1 UNALTERED DIORITE: Includes some monzonite, but dominantly dioritic in composition

~~~ Major fault

Geologic contact

Fault slip

Fault orientation: inclined, vertical

Joint orientation: inclined, vertical

Area of outcrop

• Rock samples collected by J. Nebocat (July, 1995, May, 1997); R. Tejada (Aug, 1999.)

• Rock Samples collected by Carlos E. Villafuerte (1994, 1995)

>200 PPM copper

Mal Malachite

LRC−2 Existing R.C./DDH site

Existing road/proposed road

SCALE 1:5000

DATE (REV.) FEB. 9, 2004

DRAWN BY JN

FIGURE MAP 2

LARA EXPLORATION LTD.

LARA 2A & 4 CLAIMS
CU GEOCHEMISTRY & DRILL SITES

0   125   250   375   500 M

Contour interval: 25 meters